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THE MECHANICAL PROPERTY DATA BASE FROM AN  
AIR FORCE/INDUSTRY COOPERATIVE TEST PROGRAM ON ADVANCED  
ALUMINUM ALLOYS (WELDALITE<sup>tm</sup> 049 RX815 PLATE (2095-T8))

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May 1993

Interim Report for Period February 1991 - December 1992

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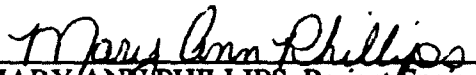
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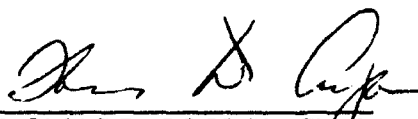
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## PREFACE

This report was prepared by the Materials Engineering Branch (WL/MLSE), Systems Support Division, Materials Directorate, Wright Laboratory, Wright-Patterson Air Force Base, Ohio, under Project 2418, "Metallic Structural Materials," Task 241807, "Systems Support," Work Unit 24180703, "Engineering and Design Data."

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## SECTION I

### INTRODUCTION

High performance aerospace systems are dependent on materials that are lighter, have improved mechanical properties, and/or offer a cost savings. Aluminum alloys that met these criteria were the newly developed aluminum-lithium alloys and the second generation powder metallurgy alloys.

In 1985, the Air Force along with the aerospace community found it important to investigate the potential of these promising aluminum alloys. A cooperative program was formed by the Wright Laboratory Materials Directorate, Systems Support Division, and a number of aerospace industries. The Air Force would obtain the test material from the producers, compile the test data, and submit reports to the participants. The participants agreed to support the program by performing mechanical property tests which includes tension, compression, bearing, shear, fracture toughness, and fatigue related properties (S/N, da/dn). The Air Force elected to perform spectrum fatigue crack growth testing on most alloys. A list of participants is shown in the following table.

This interim report contains the aluminum-lithium alloy Weldalite<sup>tm</sup> 049 RX815 0.5-inch-thick plate produced by Reynolds Metals Company. The Weldalite<sup>tm</sup> 049 RX815 alloy has been registered as 2095 with the Aluminum Association. Comparisons to other materials, and ranking of materials are generally avoided since each potential application may be based on different evaluation criteria.

TABLE

Participants and Advanced Aluminum Alloys  
in the Cooperative Test Program

PARTICIPANTS	ALUMINUM LITHIUM ALLOYS												P/M ALUMINUM ALLOYS						
	PECHINEY	ALCAN	IncoMAP	ALCOA	REYNOLDS	KAISER	ALCOA												
	2091 - T3 Sheet (0.063")	2091 - T351 Plate (0.420")	2091 - T6 Forging	8090 - T651 T Extrusion	8090 - T651 Extrusion	8090 - T8771 Plate (1.75")	PM IN905XL Forging	PM AL905XL Forging	2091 - T3 Sheet (0.063")	2091 - T3 Sheet (0.144")	2091 - T8 Plate (0.50")	8090 Extrusion	Weldable 049 RX815 Plate (0.5")	7064 - T74511 Extrusion	7064 - T74 Forging	CW67 Sheet (0.063")	CW67 Plate (0.40")	CW67 Extrusion	CW67 Forging
Air Force WPAFB, OH	x				x	x	x	x	x	x	x	x	x	x	x		x	x	
Army, MA												x	x						
AVCO, TN									x										
Boeing, WA	x	x	x	x															
Douglas Aircraft, CA								x	x	x	x	x	x						
General Dynamics, CA	x	x							x	x	x		x						
General Dynamics, TX	x	x	x	x			x		x	x	x	x							
Grumman Aerospace, NY	x	x			x		x							x	x		x	x	
Jet Propulsion, CA								x					x						
Lockheed, CA	x				x			x	x		x								
Lockheed, GA		x			x				x	x					x			x	
LTV, TX	x		x				x	x	x			x		x	x		x		
Martin Marietta, LA	x	x	x	x	x	x	x	x	x	x	x	x		x	x	x	x	x	x
McDonnell Douglas Astro, CA													x						
McDonnell Douglas Helicopter, AR								x											
McDonnell Douglas Missile Sys, MO													x						
McDonnell Aircraft, MO	x						x	x	x						x	x		x	
NASA, VA					x		x	x					x						
Naval Air Development Center	x		x					x			x							x	
Northrop, CA	x	x			x	x	x	x	x	x	x	x	x	x					
Sikorsky, CT							x		x						x		x		x
Sundstrand, IL													x						
Wyman-Gordon								x											

## SECTION II

### MATERIALS AND TESTS

The Weldalite<sup>TM</sup> 610 KX815 (2095) 0.5-inch-thick plate was received the first quarter of 1991. The 2095 was received in the T8 condition. This alloy is considered to be a damage tolerant, medium strength aluminum-lithium alloy. A chemical analysis was performed on the 2095 and the alloy chemistry is shown below.

<u>Element</u>	<u>Weight %</u>	<u>Element</u>	<u>Weight %</u>
Copper	4.17	Iron	0.057
Lithium	1.30	Nickel	0.0030
Magnesium	0.339	Titanium	0.028
Silicon	0.038	Zirconium	0.126
Silver	0.334	Aluminum	Balance

Basic mechanical properties (tension, compression, bearing, etc) were tested according to ASTM standards, unless otherwise specified. General Dynamics generated hardness and conductivity data. Constant amplitude fatigue crack growth tests were conducted according to ASTM E647 standard. Northrop Corporation performed constant amplitude fatigue crack growth test using K controlled methods. A T-38 LIF (lead-in-fighter) spectrum test was performed by Northrop Corporation. The spectrum specimen was not precracked but contained a countersunk hole to simulate a crack initiating from a fastener hole. The Army evaluated the ballistic performance of the material. The Army and Northrop Corporation have corrosion tests in process.

## SECTION III

### PRESENTATION

Each participant compiled a data package which contained the data they generated. Some of these data packages contain discussions, and in other cases, only the data were provided. The tensile, compression, bearing, shear, and fracture toughness data from each package were put in tabular form. Fatigue, fatigue crack growth, spectrum fatigue crack growth, hardness, and conductivity data were placed in tabular and graphical form. Ballistic performance data were put in text and graphical form.

## SECTION IV

### RESULTS AND DISCUSSION

The data generated by the participants on the 2095-T8 0.5 inch thick plate are shown in Tables I1 thru I36 and Figures I1 thru I15.

TABLE 11  
TENSILE RESULTS AT t/2 LOCATION FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	TEST TEMP (DEGREES F)	ORIENT- ATION	ULTIMATE STRENGTH (KSI)	YIELD STRENGTH (KSI)	ELONG (%)	RA (%)	E (MSI)
MCDONNELL DOUGLAS, MO	RT	LONG	89.7 88.4 86.8	85.7 84.3 81.1	12.0 12.0 12.0	23.7 19.7 26.4	10.9 10.8 11.4
SUNDSTRAND	RT	LONG	89.4 89.4 89.9	83.4 81.2 83.7	13.1 12.8 13.0	19.2 20.1 19.3	
ARMY-MTL	RT	LONG	88.6 88.2 87.7	81.9 81.3 80.4	12.9 11.7 12.9		10.8 10.9 10.4
GENERAL DYNAMICS	RT	LONG	88.1 89.2 89.1	82.5 84.9 84.6	10.7 11.0 10.0	17.1 21.3 17.6	11.0 11.0 11.2
NASA-LANGLEY	RT	LONG	88.0 84.9 85.0	81.2 75.6 77.2	12.3 9.6 9.6		11.2 11.3 11.3
NORTHROP	RT	LONG	89.7 88.1 89.0	83.6 80.6 81.8	13.9 13.0 13.6		11.5 11.1 11.0
AIR FORCE(*)	RT	LONG	89.4	83.1	7.4	27.0	
MCDONNELL DOUGLAS, CA	RT	LONG	84.0 82.5 82.7	77.9 76.0 77.1	12.0 13.0 10.0		
AVERAGE			87.6	81.3	11.7	21.1	11.1
STANDARD DEVIATION			2.2	2.9	1.6	3.5	0.3

(\*): TEST SECTION DIAMETER = 0.16"

TABLE 12

TENSILE RESULTS AT t/2 LOCATION FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	TEST TEMP (DEGREES F)	ORIENT- ATION	ULTIMATE STRENGTH (KSI)	YIELD STRENGTH (KSI)	ELONG (%)	RA (%)	E (MSI)
MCDONNELL DOUGLAS, MO	RT	L TRANS	87.0	80.8	11.0	23.8	11.1
			87.0	81.1	11.0	26.8	10.8
			86.8	80.8	11.0	28.4	10.9
SUNDSTRAND	RT	L TRANS	86.3	79.0	12.0	25.1	
			85.8	78.3	12.7	25.7	
			86.2	79.2	13.4	27.3	
ARMY-MTL	RT	L TRANS	84.7	75.4	14.1		10.8
			85.6	76.8	13.6		10.2
			84.9	75.7	15.0		10.7
GENERAL DYNAMICS	RT	L TRANS	84.0	75.6	11.4	21.9	11.0
			86.1	79.1	11.0	22.1	10.7
			83.8	75.4	11.0	29.7	10.8
NASA-LANGLEY	RT	L TRANS	84.8	76.4		13.1	11.3
			87.2	80.1		9.1	11.1
			87.3	80.3		14.5	11.2
NORTHROP	RT	L TRANS	85.7	75.9	14.7		11.6
			87.0	78.5	14.6		11.6
			85.2	75.3	15.5		11.1
AIR FORCE(*)	RT	L TRANS	88.9	82.4	8.8	31.0	
MCDONNELL DOUGLAS, CA	RT	L TRANS	81.2	71.7	14.5		
			80.5	71.0	14.5		
			81.8	73.0	14.0		
AVERAGE			85.4	77.4	12.8	23.0	11.0
STANDARD DEVIATION			2.1	3.1	1.9	6.8	0.4

(\*): TEST SECTION DIAMETER = 0.16"

TABLE I3

TENSILE RESULTS AT  $t/2$  LOCATION FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	TEST TEMP (DEGREES F)	ORIENT- ATION	ULTIMATE STRENGTH (KSI)	YIELD STRENGTH (KSI)	ELONG (%)	RA (%)	E (MSI)
MCDONNELL	RT	45	77.0	70.6	14.0	36.6	11.4
DOUGLAS			77.2	70.1	16.0	39.1	10.9
			76.3	69.2	17.0	39.3	10.8
AIR FORCE(*)	RT	45	75.5	69.0	8.9	41.7	9.9
		AVERAGE	76.5	69.7	14.0	39.2	10.8
		STANDARD DEVIATION	0.8	0.8	3.6	2.1	0.6

(\*): TEST SECTION DIAMETER = 0.16"

TABLE I4

TENSILE RESULTS AT  $t/2$  LOCATION FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	TEST TEMP (DEGREES F)	ORIENT- ATION	ULTIMATE STRENGTH (KSI)	YIELD STRENGTH (KSI)	ELONG (%)	RA (%)	E (MSI)
AIR FORCE	-321(*)	LONG	108.0	97.5		22.0	12.0
		L TRANS	104.0	93.8	9.6	26.0	11.7
	-150	45	95.4	89.9	12.6	25.0	11.0
	-100(*)	LONG	92.3	86.2	8.8	27.0	11.0
		45	78.7	71.5	11.4	21.6	11.5
		L TRANS	91.9	85.0	8.0	26.0	
	-40	45	90.2	83.1	12.3	25.3	10.1
	0	45	89.2	82.2	11.1	22.6	10.0
	150	45	87.5	82.9	11.4	29.2	11.4
			88.7	84.8	11.9	27.7	11.4
	200	45	78.9	78.1	16.4	47.3	10.7
			79.7	78.6	17.2	47.8	11.5

(\*): TEST SECTION DIAMETER = 0.16"



TABLE 15

TENSILE RESULTS AT t/2 LOCATION FOR REYNOLDS  
 2095-T8 PLATE (0.5" X 24" X 48")  
 (1000 HR EXPOSURE @ 350F)

COMPANY	TEST TEMP (DEGREES F)	ORIENT- ATION	ULTIMATE STRENGTH (KSI)	YIELD STRENGTH (KSI)	ELONG (%)	RA (%)	E (MSI)
AIR FORCE	RT	45	70.4	58.3	8.1	22.9	11.2
			70.1	58.0	8.2	23.8	11.3
		AVERAGE	70.3	58.1	8.2	23.3	11.2
		STANDARD DEVIATION	0.2	0.2	0.1	0.6	0.1

TABLE I6

COMPRESSION RESULTS AT  $t/2$  LOCATION FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	TEST TEMPERATURE (DEGREES F)	ORIENTATION	COMPRESSIVE YIELD STRENGTH (KSI)	COMPRESSIVE MODULUS (MSI)
MCDONNELL DOUGLAS, MO	RT	LONG	73.8 75.3 76.1	11.1 10.9 11.1
SUNDSTRAND	RT	LONG	73.1 73.3 73.8	12.0 11.8 11.7
GENERAL DYNAMICS	RT	LONG	77.0 79.0 80.0	11.3 11.6 11.4
NASA-LANGLEY	RT	LONG	62.3	11.4
NORTHROP	RT	LONG	70.9 72.2 76.7	12.2 12.1 11.9
MCDONNELL DOUGLAS, CA	RT	LONG	68.1 69.1 69.6	11.0 11.5 11.7
AVERAGE			73.1	11.6
STANDARD DEVIATION			4.5	0.4

TABLE I7

COMPRESSION RESULTS AT t/2 LOCATION FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	TEST TEMPERATURE (DEGREES F)	ORIENTATION	COMPRESSIVE YIELD STRENGTH (KSI)	COMPRESSIVE MODULUS (MSI)
MCDONNELL DOUGLAS, MO	RT	L TRANS	79.5 78.5 79.1	11.8 11.8 11.6
SUNDSTRAND	RT	L TRANS	79.4 79.0 77.6	11.6 11.5 12.7
GENERAL DYNAMICS	RT	L TRANS	79.2 80.6 80.4	11.4 11.6 12.0
NASA-LANGLEY	RT	L TRANS	75.1 77.0 76.0	11.4 11.5 11.4
NORTHROP	RT	L TRANS	79.4 75.9 73.5	11.9 12.1 12.2
MCDONNELL DOUGLAS, CA	RT	L TRANS	72.9 72.3 73.2	14.0 13.5 13.8
AVERAGE			77.1	12.1
STANDARD DEVIATION			2.8	0.8

TABLE 18

COMPRESSION RESULTS AT  $t/2$  LOCATION FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	TEST TEMPERATURE (DEGREES F)	ORIENTATION	COMPRESSIVE YIELD STRENGTH (KSI)	COMPRESSIVE MODULUS (MSI)
MCDONNELL	RT	45	70.5	11.1
DOUGLAS			70.3	11.0
			72.2	10.9
		AVERAGE	71.0	11.0
		STANDARD DEVIATION	1.0	0.1

TABLE 19

COMPRESSION RESULTS AT  $t/2$  LOCATION FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	TEST TEMPERATURE (DEGREES F)	ORIENTATION	COMPRESSIVE ULT STRENGTH (KSI)	COMPRESSIVE MODULUS (MSI)
ARMY-MTL	RT	LONG	111.2	
			107.2	
			110.7	
		AVERAGE	109.7	
		STANDARD DEVIATION	2.2	
ARMY-MTL	RT	L TRANS	115.4	
			119.0	
			114.7	
		AVERAGE	116.4	
		STANDARD DEVIATION	2.3	

TABLE I10

PIN SHEAR RESULTS FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	ORIENTATION	SHEAR STRENGTH (KSI)
ARMY-MTL	LONG	49.5
		48.8
		49.7
NORTHROP	LONG	45.7
		46.6
		46.0
	AVERAGE	47.7
	STANDARD DEVIATION	1.8

TABLE I11

RIVET SHEAR RESULTS FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	ORIENTATION	SHEAR STRENGTH (KSI)
ARMY-MTL	L TRANS	49.0
		48.5
		47.7
	AVERAGE	48.4
	STANDARD DEVIATION	0.7

TABLE 112  
TORSIONAL SHEAR RESULTS FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	ORIENTATION	SHEAR STRENGTH (KSI)
SUNDSTRAND	LONG	47.1
		46.4
		45.1
	AVERAGE	46.2
	STANDARD DEVIATION	1.0
SUNDSTRAND	L TRANS	45.4
		45.1
		46.8
	AVERAGE	45.8
	STANDARD DEVIATION	0.9

TABLE I13  
 AMSLER DOUBLE SHEAR RESULTS FOR REYNOLDS  
 2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	ORIENTATION	SHEAR STRENGTH (KSI)
NASA-LANGLEY	L-S	44.4
		46.3
		47.7
	AVERAGE	46.1
	STANDARD DEVIATION	1.7
NASA-LANGLEY	T-S	47.5
		45.6
		45.0
	AVERAGE	46.0
	STANDARD DEVIATION	1.3

TABLE I14

BEARING RESULTS FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	ORIENTATION	e/D	BEARING		BEARING	
			ULT.	STR.	YIELD	STR.
			(KSI)		(KSI)	
MCDONNELL	LONG	1.5	128.0		106.0	
DOUGLAS, MO			119.0		100.0	
			122.0		103.0	
NASA-LANGLEY	LONG	1.5	123.1		99.2	
			119.4		98.4	
			120.6		100.3	
NORTHROP	LONG	1.5	156.4		116.5	
			154.3		114.3	
			153.6		113.7	
MCDONNELL	LONG	1.5	120.2		102.1	
DOUGLAS, CA			121.1		101.9	
			121.1		101.5	
AVERAGE			129.9		104.7	
STANDARD DEVIATION			15.2		6.4	

TABLE I15

BEARING RESULTS FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	ORIENTATION	e/D	BEARING		BEARING	
			ULT.	STR.	YIELD	STR.
			(KSI)		(KSI)	
MCDONNELL	45	1.5	128.0		106.0	
DOUGLAS, MO			131.0		110.0	
			135.0		111.0	
AVERAGE			131.3		109.0	
STANDARD DEVIATION			3.5		2.6	



TABLE I16

BEARING RESULTS FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	ORIENTATION	e/D	BEARING	
			ULT. STR. (KSI)	YIELD STR. (KSI)
MCDONNELL DOUGLAS, MO	L TRANS	1.5	125.0 129.0 131.0	106.0 105.0 107.0
NASA-LANGLEY	L TRANS	1.5	122.2 124.2 124.7	98.4 101.6 99.4
NORTHROP	L TRANS	1.5	158.7 160.4 160.2	121.1 120.6 128.5
MCDONNELL DOUGLAS, CA	L TRANS	1.5	121.7 121.7 120.5	100.4 98.3 97.3
AVERAGE			133.3	107.0
STANDARD DEVIATION			16.3	10.6

TABLE I17  
BEARING RESULTS FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	ORIENTATION	e/D	BEARING ULT. STR. (KSI)	BEARING YIELD STR. (KSI)
MCDONNELL DOUGLAS, MO	LONG	2.0	164.0 159.0 158.0	128.0 131.0 130.0
NASA-LANGLEY	LONG	2.0	148.0 146.7	114.5 111.0 112.3
NORTHROP	LONG	2.0	183.1 183.6 182.5	120.6 123.1 122.7
MCDONNELL DOUGLAS, CA	LONG	2.0	157.5 156.5 157.4	119.6 124.1 120.2
AVERAGE			163.3	121.4
STANDARD DEVIATION			13.6	6.5

TABLE I18  
BEARING RESULTS FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	ORIENTATION	e/D	BEARING ULT. STR. (KSI)	BEARING YIELD STR. (KSI)
MCDONNELL DOUGLAS, MO	45	2.0	172.0 166.0 169.0	141.0 136.0 138.0
AVERAGE			169.0	138.3
STANDARD DEVIATION			3.0	2.5

TABLE I19

BEARING RESULTS FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	ORIENTATION	e/D	BEARING	
			ULT. STR. (KSI)	YIELD STR. (KSI)
MCDONNELL DOUGLAS, MO	L TRANS	2.0	163.0 160.0 166.0	132.0 137.0 137.0
NASA-LANGLEY	L TRANS	2.0		116.4 116.6 116.1
NORTHROP	L TRANS	2.0	186.9 188.5 189.8	126.7 131.2 127.5
MCDONNELL DOUGLAS, CA	L TRANS	2.0	155.4 158.9 156.8	122.1 124.6 122.9
AVERAGE			166.8	125.8
STANDARD DEVIATION			14.4	7.5

TABLE I20

**FRACTURE TOUGHNESS RESULTS FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")**

COMPANY	ORIENTATION	KIC (KSI in <sup>0.5</sup> )	Kq (KSI in <sup>0.5</sup> )	COMMENT
MCDONNELL	L-T		26.3	(1)
DOUGLAS			22.8	(2)
SUNDSTRAND	L-T	30.2 30.0		
ARMY-MTL	L-T	26.8		
			37.3	(2), (3)
			33.3	(2)
			36.4	(2), (3)
			33.7	(2)
GENERAL	L-T		33.5	(2)
DYNAMICS			30.7	(2)
			30.1	(2)
NASA-LANGLEY	L-T	27.0		
			25.3	(2)
NORTHROP	L-T		37.7	(3)
			40.4	(3)
			43.3	(3)
	AVERAGE	28.5	33.1	
	STANDARD DEVIATION	1.8	6.0	

(1): INVALID DUE TO SURFACE CRACK LENGTH MEASUREMENTS  
EXCEEDED 10% OF AVERAGE CRACK LENGTH

(2): INVALID DUE TO  $P_{max}/P_q > 1.10$

(3): INVALID DUE TO  $a \text{ \& } B > 2.5(Kq/Y_S)^{**2}$

TABLE I21  
FRACTURE TOUGHNESS RESULTS FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	ORIENTATION	KIC (KSI in <sup>0.5</sup> )	Kq (KSI in <sup>0.5</sup> )	COMMENT
MCDONNELL DOUGLAS	T-L	29.6	25.8	(1)
SUNDSTRAND	T-L	29.1 29.0		
ARMY-MTL	T-L		40.2 35.6 35.0 35.9 36.9 35.5	(2), (3) (3) (2), (3) (2), (3) (2), (3) (3)
GENERAL DYNAMICS	T-L	31.4	29.4 29.2	(2) (2)
NASA-LANGLEY	T-L	24.4		
NORTHROP	T-L		38.7 38.3 37.9	(3) (3) (3)
	AVERAGE	28.7	34.9	
	STANDARD DEVIATION	2.6	4.4	

(1): INVALID DUE TO SURFACE CRACK LENGTH MEASUREMENTS  
EXCEEDED 10% OF AVERAGE CRACK LENGTH

(2): INVALID DUE TO  $P_{max}/P_q > 1.10$

(3): INVALID DUE TO  $a \text{ \& } B > 2.5(Kq/Y_S)^{**2}$

TABLE I22

FRACTURE TOUGHNESS RESULTS FOR REYNOLDS  
2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	ORIENTATION	K <sub>IC</sub>	K <sub>q</sub>	COMMENT
		(KSI in <sup>-0.5</sup> )	(KSI in <sup>-0.5</sup> )	
MCDONNELL	45		25.4	(1)
DOUGLAS		23.6		

(1): INVALID DUE TO SURFACE CRACK LENGTH MEASUREMENTS  
EXCEEDED 10% OF AVERAGE CRACK LENGTH

TABLE I23

Hardness & Conductivity Results for 2095-T8  
0.5 Inch Plate. General Dynamics, CA

Alloy/Product Form	Hardness (R <sub>B</sub> Scale)	Conductivity (% IACS)
Weldalite 2095-T8 0.50 Inch Plate	See Figure	22 (a) 17 (b)
(a) as received mill surface		
(b) machined surface		

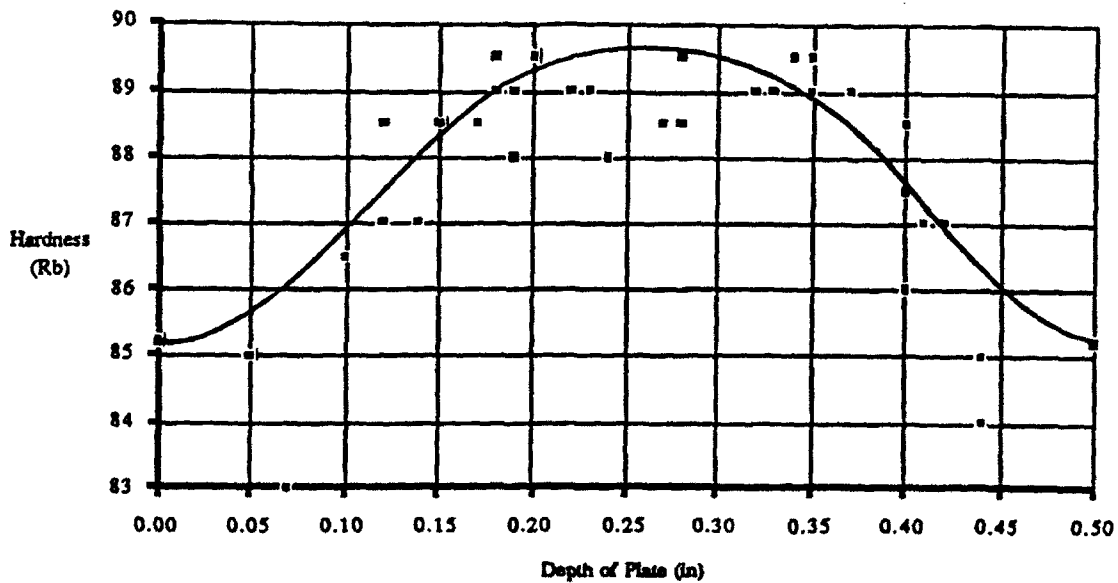
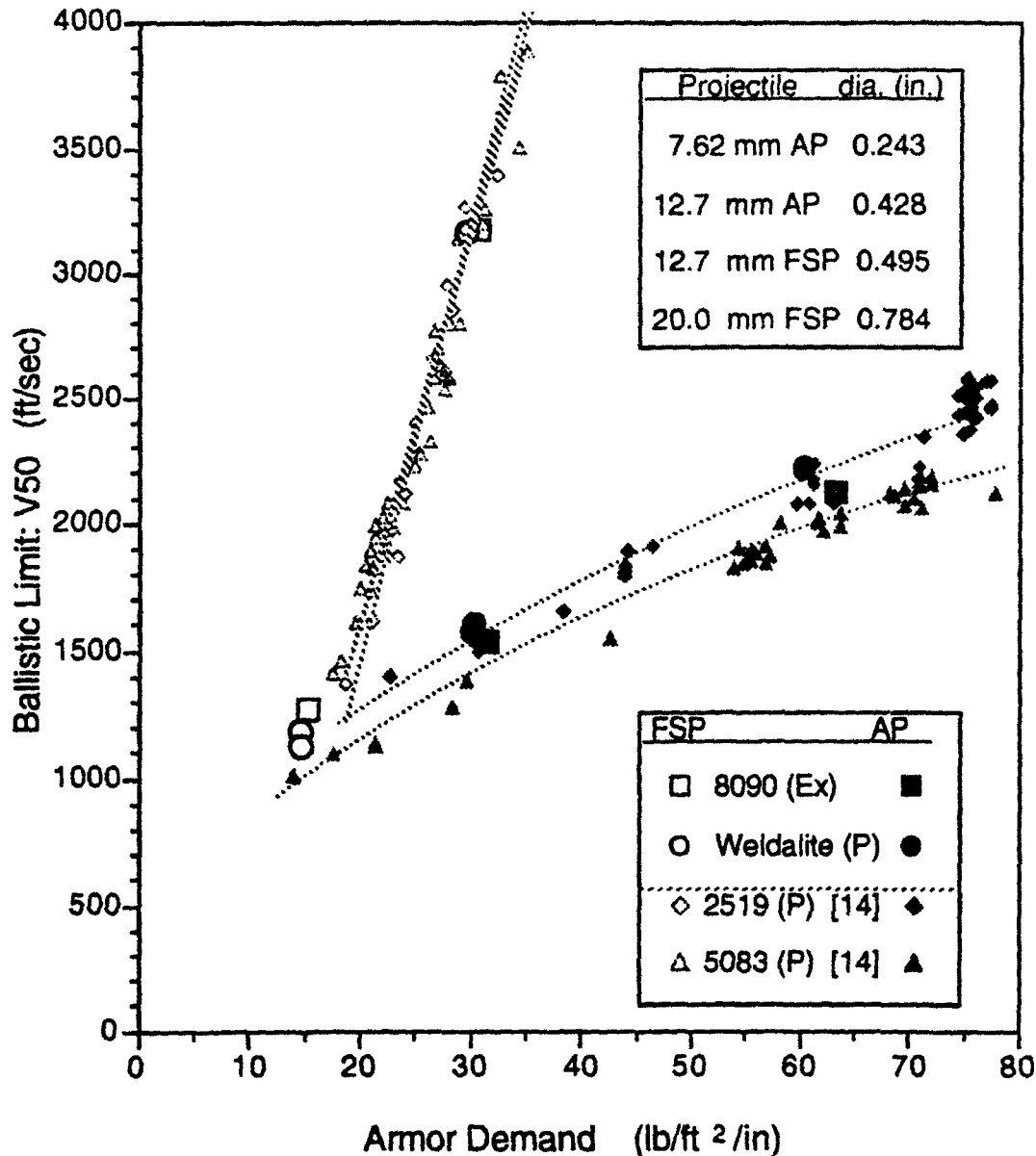


Figure I1. Hardness profile through 2095-T8  
0.5 Inch Plate. General Dynamics, CA.



Both 8090 extrusions (Ex) and Weldalite plates (P) provided enhanced ballistic performance over 2519 and 5083 Al alloys. The  $V_{50}$  ballistic limits against AP and FSP projectiles at 0° obliquity are plotted versus Armor demand. The Armor demand is defined as the (density x thickness) / projectile diameter. The ballistic data for different caliber projectiles superimpose on single curves for either AP or FSP projectiles when plotted against armor demand. This technique allows designers to evaluate ballistic performance as a function of projectile type rather than for individual munitions. The AP and FSP projectile diameters are included as inserts in the plot. Ballistic data for 2519 and 5083 are included as the high and low ends of aluminum alloys currently being considered for structural armor applications. The lower set of 8090 and Weldalite data points for both AP and FSP projectiles represent 0.5 inch ballistic targets. The second series of data points for each projectile type represent stacked plates to provide 1.0 inch thickness. The ballistic limits of both AL-Li alloys are attributed to the witness plate being perforated by spalling rather than by the projectile exiting the target.

Figure I2. Ballistic limit ( $V_{50}$ ) versus Armor Demand at 0° obliquity against Armor Piercing (AP) and Fragment Simulating Projectiles (FSP). Army.



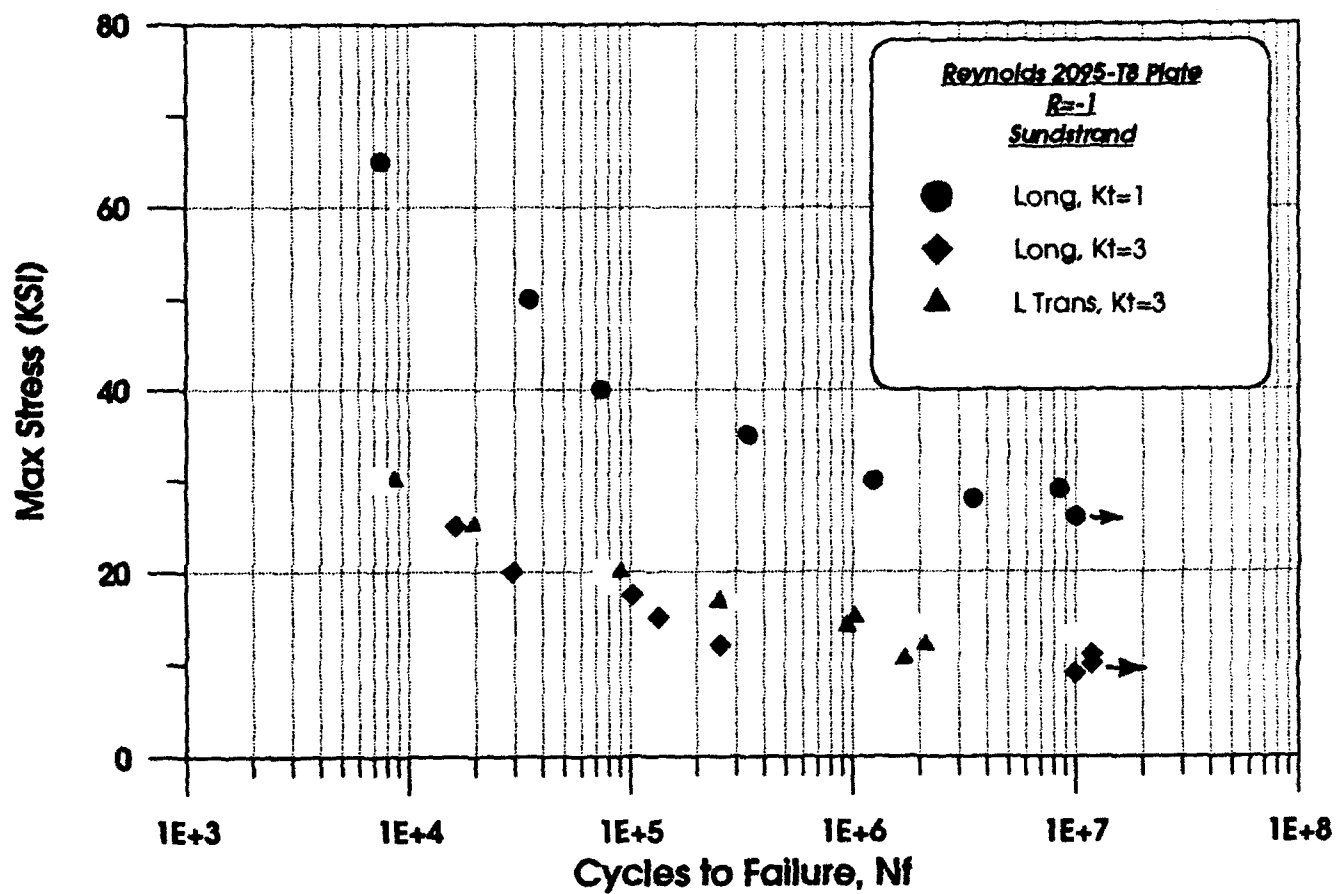


Figure I3. Fatigue Results for 2095-T8 0.5 Inch Plate ( $R = -1$ ,  $K_t = 1.0$  and  $K_t = 3.0$ ) and 2095-T6 ( $R = -1$  and  $K_t = 3$ )

TABLE I24

FATIGUE RESULTS WITH  $R=-1.0$  AND  $K_t=1.0$  FOR  
REYNOLDS 2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	ORIENTATION	STRESS (KSI)	CYCLES
SUNDSTRAND	LONG	65.0	7,500
		50.0	34,950
		40.0	73,820
		35.0	338,910
		30.0	1,240,950
		29.0	8,461,080
		28.0	3,489,830
		26.0	10,000,000 *

(\*): RUN OUT

TABLE I25

FATIGUE RESULTS WITH  $R=-1.0$  AND  $K_t=3.0$  FOR  
REYNOLDS 2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	ORIENTATION	STRESS (KSI)	CYCLES
SUNDSTRAND	LONG	25.0	16,300
		20.0	29,460
		17.5	102,580
		15.0	133,920
		12.0	253,810
		11.0	11,796,000 *
		10.0	11,913,000 *
		9.0	10,000,000 *

(\*): RUN OUT

TABLE I26

FATIGUE RESULTS WITH R=-1.0 AND Kt=3.0 FOR  
REYNOLDS 2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	ORIENTATION	STRESS (KSI)	CYCLES
SUNDSTRAND	L TRANS	30.0	8,620
		25.0	19,690
		20.0	90,000
		17.0	254,530
		15.0	1,024,210
		14.0	943,790
		12.0	2,110,280
		10.5	1,715,500

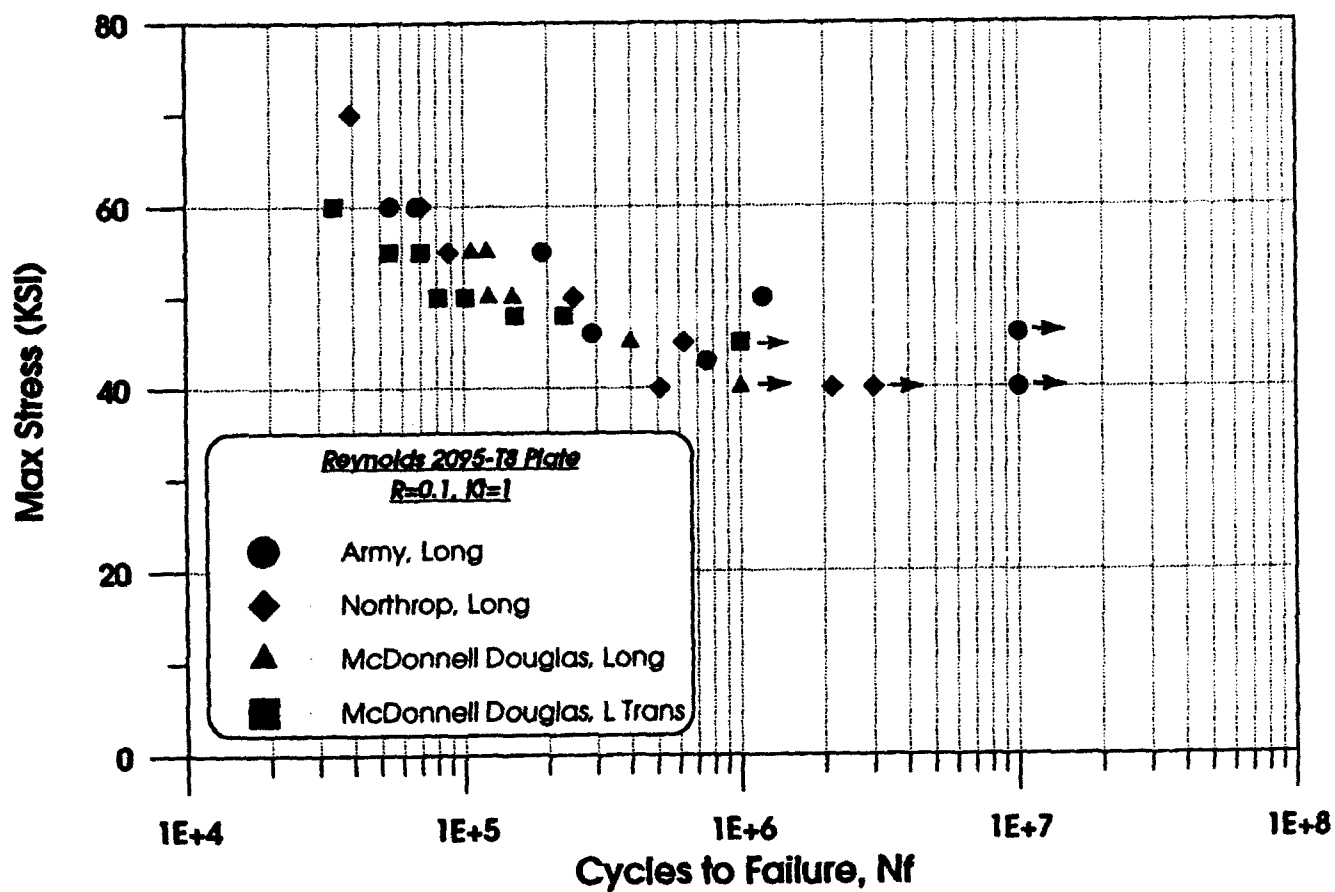


Figure I4. Fatigue Results for 2095-T8 0.5 Inch Plate ( $R = 0.1$  and  $K_t = 1.0$ )

TABLE I27

FATIGUE RESULTS WITH R=0.1 AND Kt=1.0 FOR  
REYNOLDS 2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	ORIENTATION	STRESS (KSI)	CYCLES
ARMY-MTL	LONG	60.0	54,220
		60.0	67,580
		55.0	191,520
		50.0	1,205,760
		46.0	290,042
		46.0	10,026,880 *
		43.0	754,000
		40.0	10,010,000 *
NORTHROP	LONG	70.0	39,420
		60.0	70,550
		55.0	87,944
		50.0	247,950
		45.0	623,760
		40.0	511,870
		40.0	3,000,000 *
		40.0	2,135,840
MCDONNELL DOUGLAS, CA	LONG	55.0	106,010
		55.0	120,950
		50.0	149,620
		50.0	122,970
		45.0	398,910
		45.0	398,300
		40.0	1,000,000 *
		40.0	1,000,000 *
MCDONNELL DOUGLAS, CA	L TRANS	60.0	34,170
		55.0	53,870
		55.0	69,800
		50.0	101,060
		50.0	80,470
		48.0	153,080
		48.0	229,570
		45.0	1,000,000 *
		45.0	1,000,000 *
(*) : RUN-OUT			

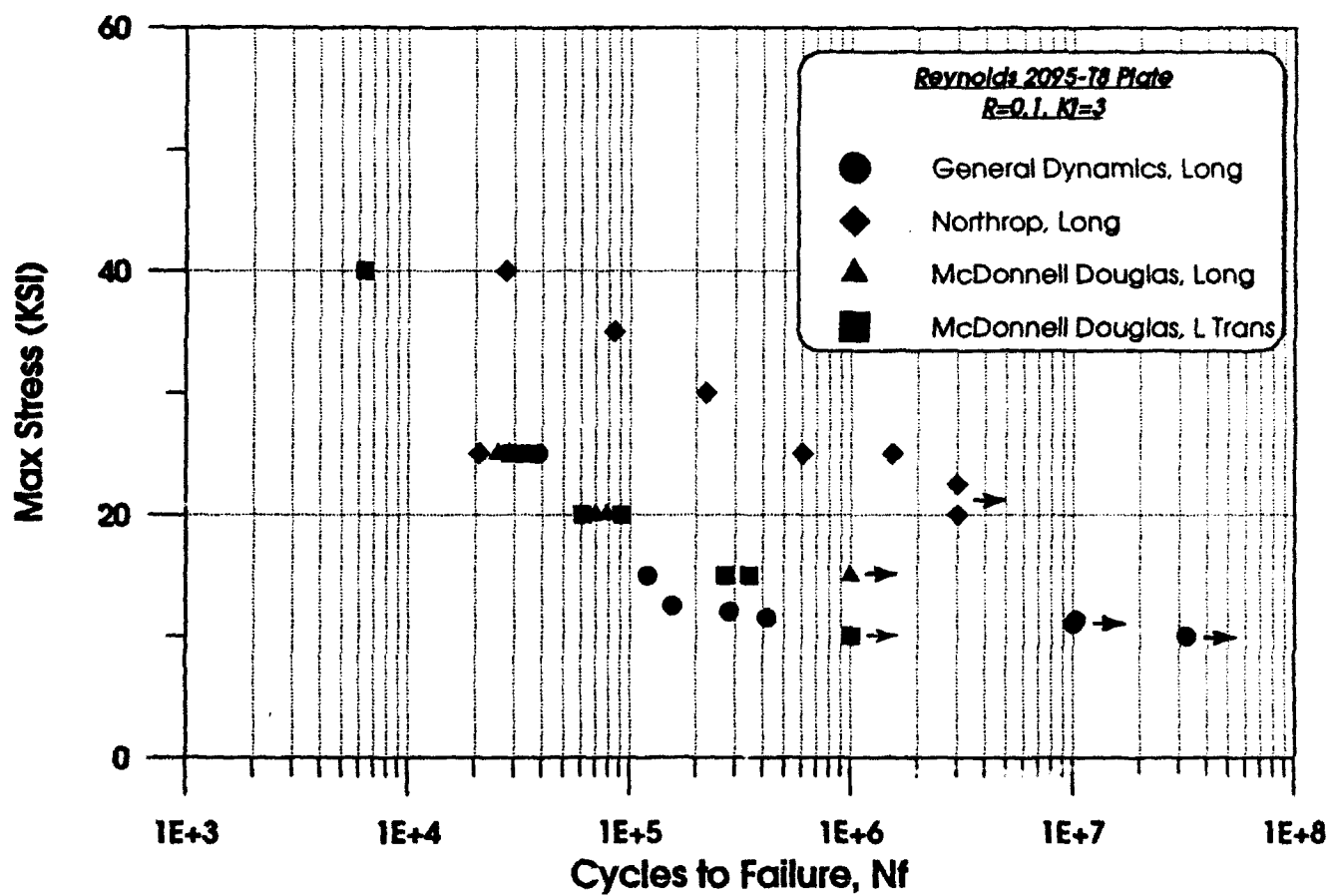


Figure I5. Fatigue Results for 2095-T8 0.5 Inch Plate ( $R = 0.1$  and  $K_t = 3$ )

TABLE I28

FATIGUE RESULTS WITH R=0.1 AND Kt=3.0 FOR  
REYNOLDS 2095-T8 PLATE (0.5" X 24" X 48")

COMPANY	ORIENTATION	STRESS (KSI)	CYCLES
GENERAL DYNAMICS	LONG	25.0	38,200
		15.0	120,600
		12.5	155,500
		12.0	281,900
		11.5	417,100
		11.3	10,240,300 *
		11.0	10,000,000 *
		10.0	32,313,000 *
NORTHROP	LONG	40.0	27,530
		35.0	84,820
		30.0	220,840
		25.0	20,830
		25.0	605,470
		25.0	1,535,480
		22.5	3,000,000 *
		20.0	3,000,000 *
MCDONNELL DOUGLAS, CA	LONG	25.0	28,540
		25.0	25,320
		20.0	78,410
		20.0	69,950
		15.0	1,000,000 *
		15.0	1,000,000 *
		10.0	1,000,000 *
		10.0	1,000,000 *
MCDONNELL DOUGLAS, CA	L TRANS	40.0	6,331
		25.0	28,860
		25.0	32,940
		20.0	60,520
		20.0	91,030
		15.0	348,180
		15.0	271,490
		10.0	1,000,000 *
		10.0	1,000,000 *

(\*): RUN-OUT

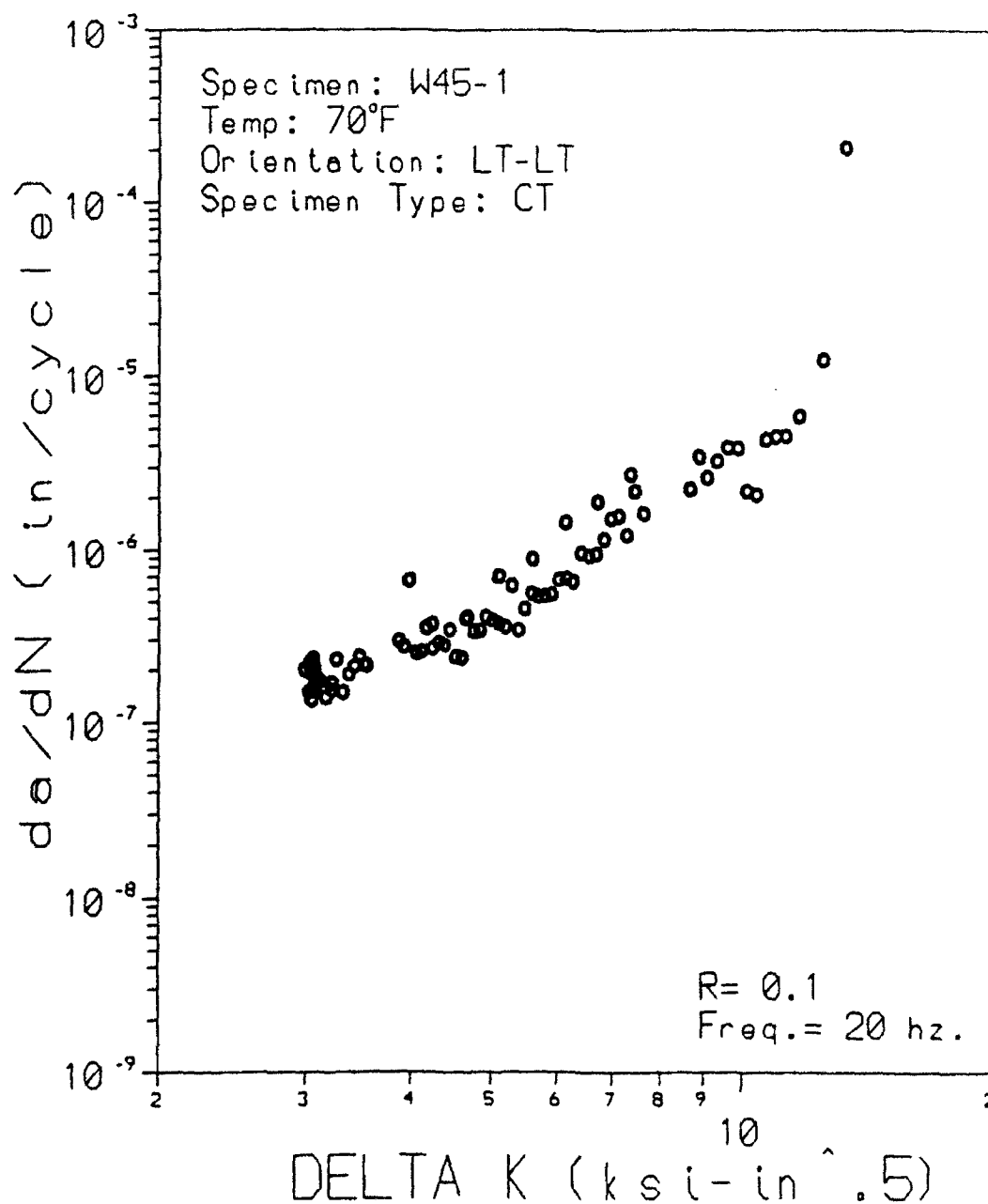


Figure I6. Fatigue Crack Growth Rate Data for 2095-T8 0.5 Inch Plate (LT-LT orientation, Specimen W45-1). Air Force.



TABLE I29

Fatigue Crack Growth Data Associated with Figure I6

WAS-1.DAT	N	da/dN (in/cycle)	da/dN (mm/cycle)	P <sub>max</sub> (ksi)	W= B=	2.003 in 0.249 in	a(c) (in)	N (cycles)	da/dN(c) (in/cycle)	da/dN(m) (mm/cycle)	da/dN(c) (in-in <sup>-1</sup> )	da/dN(m) (mm-mm <sup>-1</sup> )
0.5339	0.0	0.0000	7.23	550			0.5339	0.0	4.8	2.77E-08	7.36	4.52
0.5471	4.8	2.1053	7.31	550			0.5472	4.8	10.1	1.92E-08	4.33	4.60
0.5572	10.1	1.8785	6.67	495			0.5574	10.1	17.3	1.43E-08	4.36	4.66
0.5675	17.3	1.4362	6.08	446			0.5678	17.3	28.7	8.93E-07	4.46	4.76
0.5775	28.7	0.8745	5.55	401			0.5780	28.7	43.3	7.08E-07	4.53	4.84
0.5878	43.3	0.6907	5.06	361			0.5883	43.3	69.8	4.00E-07	4.60	4.92
0.5977	69.8	0.3957	4.61	325			0.5988	69.8	109.2	2.71E-07	4.68	5.01
0.6078	109.2	0.2544	4.20	292			0.6095	109.2	144.6	2.96E-07	4.75	5.19
0.6178	144.6	0.2940	3.83	263			0.6201	144.6	261.4	1.68E-07	4.83	5.19
0.6279	195.6	0.1968	3.50	237			0.6310	195.6	327.9	1.01E-07	4.91	5.29
0.6379	261.4	0.1530	3.19	213			0.6421	261.4	381.9	7.11E-07	4.96	5.36
0.6482	327.9	0.1539	3.07	202			0.6534	327.9	457.1	5.00E-07	5.06	5.48
0.6582	381.9	0.1861	2.95	192			0.6643	381.9	541.8	3.35E-07	5.16	5.59
0.6685	457.1	0.1338	2.99	182			0.6756	457.1	598.8	2.26E-07	5.25	5.69
0.6784	541.8	0.1193	2.98	180			0.6870	541.8	641.8	2.08E-07	5.34	5.80
0.6885	598.8	0.2101	2.99	187			0.6979	598.8	694.7	2.04E-07	5.44	5.91
0.6985	641.8	0.1942	2.98	185			0.7087	641.8	754.2	1.87E-07	5.54	6.03
0.7085	694.7	0.1883	2.99	182			0.7196	694.7	800.5	1.54E-07	5.64	6.15
0.7284	754.2	0.1712	2.99	180			0.7307	754.2	872.9	1.36E-07	5.74	6.27
0.7388	800.5	0.2166	2.99	178			0.7416	800.5	955.6	1.08E-07	5.86	6.40
0.7488	872.9	0.1367	2.98	175			0.7527	872.9	1054.6	8.34E-07	5.91	6.54
0.7488	943.3	0.1420	2.99	173			0.7638	943.3	1171.7	7.14E-07	6.07	6.67
0.7589	995.6	0.1933	2.99	171			0.7748	995.6	1256.1	5.96E-07	6.19	6.82
0.7689	1054.6	0.1702	2.99	169			0.7857	1054.6	1337.3	4.94E-07	6.32	6.96
0.7789	1117.7	0.1586	2.99	167			0.7967	1117.7	1411.1	4.13E-07	6.44	7.11
0.7890	1181.2	0.1370	2.99	164			0.8080	1181.2	1457.8	3.31E-07	6.57	7.27
0.7991	1256.1	0.1546	3.03	164			0.8181	1256.1	1534.5	2.77E-07	6.71	7.44
0.8091	1337.3	0.1233	3.07	164			0.8304	1337.3	1592.1	2.19E-07	6.86	7.62
0.8192	1411.1	0.1370	3.11	164			0.8417	1411.1	1644.4	1.90E-07	6.99	7.82
0.8292	1457.8	0.2156	3.15	164			0.8524	1457.8	1709.2	1.53E-07	7.11	8.07
0.8394	1592.1	0.1323	3.19	164			0.8638	1592.1	1775.5	1.19E-07	7.27	8.27
0.8494	1644.4	0.1743	3.23	164			0.8748	1644.4	1835.3	9.07E-07	7.44	8.44
0.8595	1699.1	0.1918	3.28	164			0.8857	1699.1	1878.8	7.70E-07	7.62	8.62
0.8695	1809.1	0.2253	3.32	164			0.8964	1809.1	1925.6	6.20E-07	7.82	8.82
0.8796	1799.2	0.2007	3.37	164			0.9073	1799.2	1975.5	5.00E-07	8.07	9.07
0.8896	1777.5	0.2628	3.74	180			0.9179	1777.5	2009.2	4.13E-07	8.27	9.27
0.8996	1793.1	0.0496	3.79	180			0.9284	1793.1	2039.2	3.31E-07	8.44	9.44
0.9096	1835.3	0.2369	3.85	180			0.9390	1835.3	2069.2	2.77E-07	8.62	9.62
0.9199	1876.8	0.2439	3.90	180			0.9498	1876.8	2099.2	2.21E-07	8.82	9.82
0.9299	1908.2	0.3410	3.96	180			0.9603	1908.2	2129.2	1.71E-07	9.07	10.07
0.9401	1924.8	0.3579	4.02	180			0.9708	1924.8	2159.2	1.36E-07	9.27	10.27
0.9503	1971.8	0.2746	4.06	180			0.9817	1971.8	2189.2	1.08E-07	9.44	10.44
0.9603	2009.1	0.2686	4.14	180			0.9923	2009.1	2219.2	8.62E-07	9.62	10.62
0.9703	2039.2	0.3315	4.20	180			1.0028	2039.2	2249.2	7.14E-07	9.82	10.82

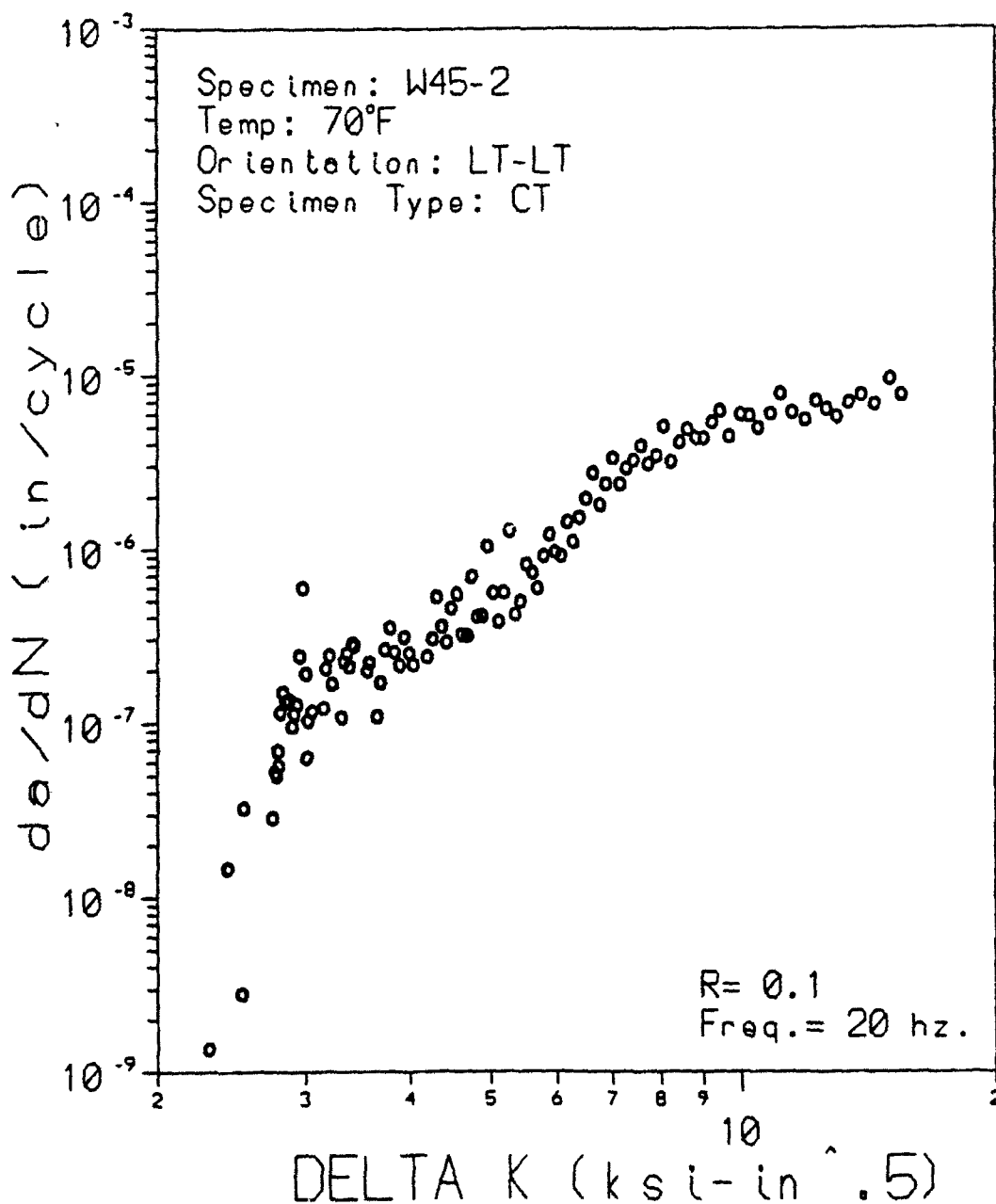


Figure I7. Fatigue Crack Growth Rate Data for 2095-T8 0.5 Inch Plate (LT-LT orientation, Specimen W45-2). Air Force.

TABLE I30

W45-2.DAT

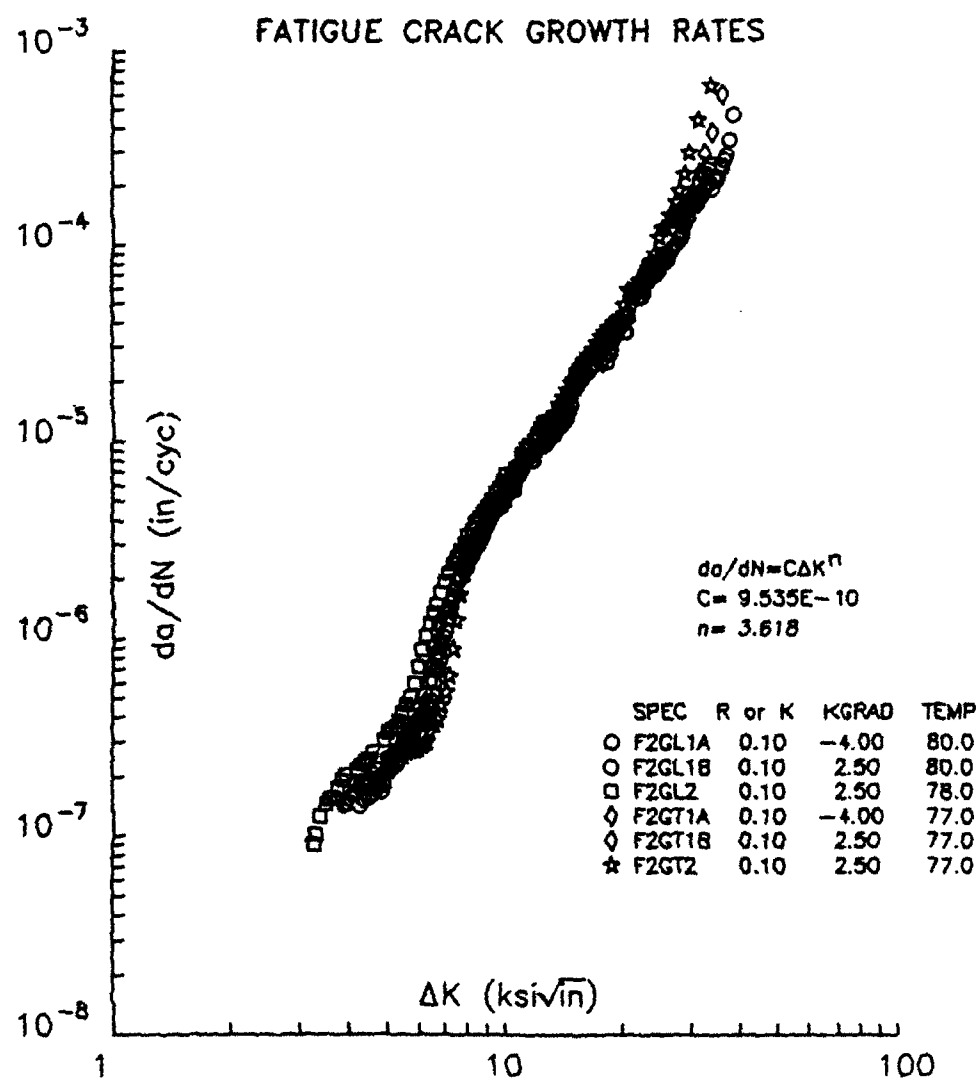


Figure 18. Fatigue Crack Growth Rate Data for 2095-T8 0.5 Inch Thick Plate (L-T and T-L orientations). Northrop.

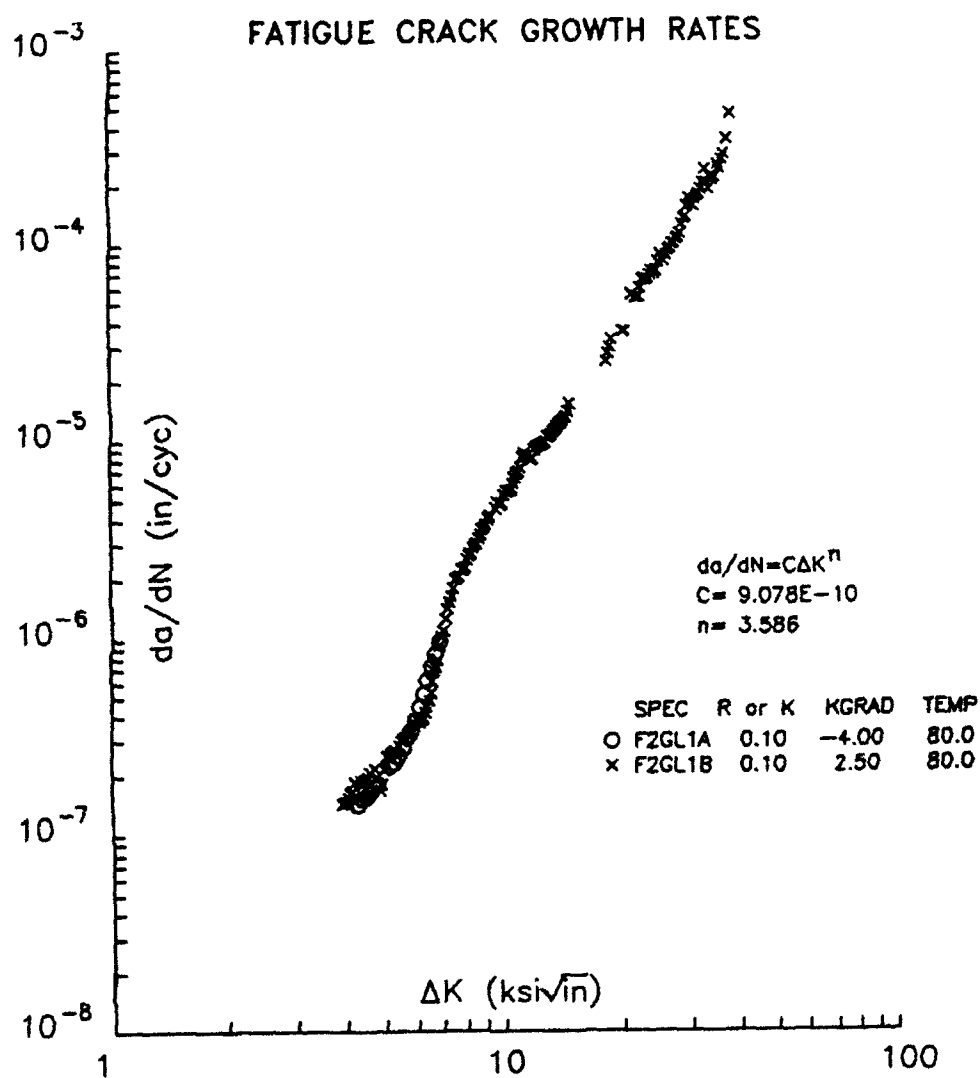


Figure 19. Fatigue Crack Growth Rate Data for 2095-T8 0.5 Inch Thick Plate (L-T orientation, KGRAD - 4.00 and 2.50). Northrop.

TABLE I31

## Fatigue Crack Growth Data Associated with Figure I9 (Specimen F2GL1A)

AUTOMATED FATIGUE CRACK  
GROWTH RATE ANALYSIS

Specimen Id.	F2GL1A	Geometry	C(T)
Contract #	WB02115N	Orientation	L-T
Material	Weldalite	Yield (ksi)	82.0
Temperature (F)	80	Modulus	11.1
Environment	Lab. air		

## Specimen Dimensions (in)

Thickness	0.495	Notch depth	0.609
Width	2.997	Gage length	1.000
Height	3.600	Alpha ratio	1.250

## Precrack Parameters

Pmax (lbs)	1471.0	Stress ratio (R)	0.10
Final a (in)	0.689	Kmax	8.00

## Test Parameters

Initial a (in)	0.689	Initial K	8.00
K-gradient	-4.00	Stress ratio (R)	0.10

K Coeff	EvB/P Coeff	Analysis Codes
0.886000	1.000980	KRP 2 0
4.640000	-4.669510	
-13.320000	18.460100	
14.720000	-236.824997	
-5.600000	1214.880000	
0.000000	-2143.570100	

## Visual Observations

EvB/P	Crack (EvB/P)	Crack (visual)	Error	CAF
19.54	0.689	0.656	-.033	1.000
20.82	0.745	0.715	-.031	1.000
21.33	0.766	0.728	-.038	1.000
21.58	0.776	0.754	-.023	1.000
21.67	0.780	0.757	-.023	1.000
23.00	0.831	0.800	-.031	1.000
23.65	0.855	0.818	-.036	1.000
24.14	0.872	0.836	-.036	1.000
25.06	0.904	0.870	-.034	1.000
27.11	0.969	0.928	-.041	1.000
29.75	1.045	1.017	-.028	1.000
92.36	1.818	1.818	-.000	1.000

Peak (lbs)	EvB/P	a (in)	N (X1)	Δa (in)	ΔN (X1)	Δa/ΔN (in/cyc)	ΔK (ksi/in)
	19.64	0.6938	4398				
1393	19.80	0.7011	11308	0.0130	13262	9.783E-07	6.89
1347	19.93	0.7067	17660	0.0118	14041	8.406E-07	6.70
1308	20.07	0.7129	25349	0.0125	17258	7.251E-07	6.55
1269	20.22	0.7193	34918	0.0126	20541	6.157E-07	6.38
1232	20.36	0.7255	45890	0.0120	22772	5.256E-07	6.23
1195	20.49	0.7312	57689	0.0117	26035	4.505E-07	6.08
1162	20.63	0.7373	71925	0.0118	30699	3.849E-07	5.94
1128	20.77	0.7430	88388	0.0118	34418	3.416E-07	5.80
1095	20.91	0.7490	106343	0.0124	39201	3.158E-07	5.66
1063	21.07	0.7554	127588	0.0123	44693	2.761E-07	5.53
1031	21.21	0.7614	151035	0.0120	48064	2.496E-07	5.39
1001	21.36	0.7674	175652	0.0121	51794	2.336E-07	5.27
974	21.51	0.7735	202829	0.0111	49535	2.245E-07	5.15
	21.64	0.7785	225187				
	21.82	0.7859	249807				
888	21.97	0.7918	282411	0.0119	66418	1.796E-07	4.77
863	22.13	0.7978	316225	0.0121	69261	1.745E-07	4.66
838	22.28	0.8038	351672	0.0118	71831	1.638E-07	4.55
814	22.43	0.8096	388056	0.0116	73904	1.574E-07	4.45
791	22.59	0.8155	425576	0.0120	78849	1.523E-07	4.34
768	22.75	0.8216	466905	0.0122	85698	1.428E-07	4.24
	22.91	0.8277	511274				
	23.08	0.8341	537843				
	23.23	0.8395	565306				

TABLE I32

Fatigue Crack Growth Data Associated with Figure I9 (Specimen F2GL1B)

AUTOMATED FATIGUE CRACK  
GROWTH RATE ANALYSIS

Specimen Id.	F2GL1B	Geometry	C(T)
Contract #	WB02115N	Orientation	L-T
Material	Weldalite	Yield (ksi)	82.0
Temperature (F)	80	Modulus	11.1
Environment	Lab. air		

## Specimen Dimensions (in)

Thickness	0.495	Notch depth	0.609
Width	2.997	Gage length	1.000
Height	3.600	Alpha ratio	1.250

## Pretcrack Parameters

Pmax (lbs)	1471.0	Stress ratio (R)	0.10
Final a (in)	0.689	Kmax	8.00

## Test Parameters

Initial a (in)	0.855	Initial K	4.10
K-gradient	2.50	Stress ratio (R)	0.10

K Coeff	EvB/P Coeff	Analysis Codes
0.886000	1.000980	KRP 2 0
4.640000	-4.669510	
-13.320000	18.460100	
14.720000	-236.824997	
-5.600000	1214.880000	
0.000000	-2143.570100	

## Visual Observations

EvB/P	Crack (EvB/P)	Crack (visual)	Error	CAF
19.54	0.689	0.656	-.033	1.000
20.82	0.745	0.715	-.031	1.000
21.33	0.766	0.728	-.038	1.000
21.58	0.776	0.754	-.023	1.000
21.67	0.780	0.757	-.023	1.000
23.00	0.831	0.800	-.031	1.000
23.65	0.855	0.818	-.036	1.000
24.14	0.872	0.836	-.036	1.000
25.06	0.904	0.870	-.034	1.000
27.11	0.969	0.928	-.041	1.000
29.75	1.045	1.017	-.028	1.000
92.36	1.818	1.818	-.000	1.000

## Comments

Date of test: 08-12-1992

**TABLE I32 (Continued)**

Specimen Id. F2GL18															Page 2	
Peak	E48/P (lbs)	a (in)	N (X1)	As (in)	AN (X1)	Δa/ΔN (in/cyc)	AK (ksi/in)	Phax (lbs)	E48/P	a (in)	N (X1)	As (in)	AN (X1)	Δa/ΔN (in/cyc)	AK (ksi/in)	
669	24.01	0.8676	106831	0.0106	73428	1.449E-07	3.86	935	30.98	1.0768	1004990	0.0091	18962	4.840E-07	6.43	
674	24.17	0.8732	146247	0.0093	63733	1.457E-07	3.91	942	31.16	1.0814	1014201	0.0093	17546	5.297E-07	6.50	
680	24.32	0.8782	208259	0.0089	63733	1.457E-07	3.96	949	31.34	1.0861	1022536	0.0095	15479	6.108E-07	6.58	
685	24.44	0.8825	195981	0.0095	60742	1.543E-07	4.00	956	31.53	1.0908	1029679	0.0091	13151	6.907E-07	6.65	
685	24.58	0.8872	241001	0.0095	61687	1.543E-07	4.05	963	31.70	1.0952	1035686	0.0087	11912	7.275E-07	6.73	
690	24.72	0.8920	271668	0.0095	58702	1.614E-07	4.10	970	31.87	1.0995	1041591	0.0089	11248	7.897E-07	6.80	
695	24.86	0.8966	299703	0.0092	55018	1.665E-07	4.15	977	32.06	1.1040	1046934	0.0091	9853	9.256E-07	6.88	
700	24.99	0.9012	326686	0.0076	41150	1.843E-07	4.14	985	32.24	1.1086	1051444	0.0091	8856	1.029E-06	6.96	
700	25.08	0.9042	340853					992	32.43	1.1132	1055790	0.0088	7892	1.109E-06	7.04	
716	25.27	0.9106	351337	0.0086	45977	1.878E-07	4.29	999	32.60	1.1174	1059335	0.0088	6876	1.276E-06	7.12	
722	25.40	0.9147	373211	0.0092	50824	1.802E-07	4.34	1007	32.79	1.1219	1062665	0.0093	6517	1.427E-06	7.20	
727	25.54	0.9192	397314	0.0091	48344	1.887E-07	4.38	1014	32.99	1.1267	1065853	0.0089	5795	1.533E-06	7.28	
732	25.68	0.9239	423034	0.0085	44229	1.913E-07	4.43	1021	33.16	1.1308	1068460	0.0086	5212	1.642E-06	7.36	
738	25.82	0.9283	445658	0.0090	45789	1.962E-07	4.48	1029	33.35	1.1352	1071065	0.0091	5087	1.812E-06	7.44	
743	25.94	0.9323	467264	0.0098	47368	2.060E-07	4.53	1036	33.56	1.1400	1073547	0.0091	4562	1.995E-06	7.52	
743	26.10	0.9373	491447	0.0098				1044	33.74	1.1443	1075626	0.0088	4357	2.028E-06	7.61	
743	26.25	0.9421	514632					1052	33.94	1.1489	1077904	0.0095	4508	2.063E-06	7.70	
760	26.54	0.9513	567212	0.0092	42714	2.164E-07	4.69	1060	34.15	1.1538	1080215	0.0095	4233	2.235E-06	7.79	
765	26.67	0.9552	583835	0.0073	36982	1.962E-07	4.74	1068	34.35	1.1583	1082137	0.0087	3878	2.236E-06	7.88	
773	26.78	0.9585	604194	0.0119	69783	1.699E-07	4.81	1076	34.54	1.1625	1084093	0.0089	3859	2.308E-06	7.97	
779	27.06	0.9671	653618	0.0153	84036	1.815E-07	4.87	1083	34.75	1.1673	1086006	0.0089	3538	2.528E-06	8.05	
788	27.28	0.9738	688230	0.0112	52470	2.140E-07	4.95	1091	34.93	1.1713	1087601	0.0085	3236	2.634E-06	8.15	
795	27.43	0.9783	705088	0.0088	35600	2.482E-07	5.02	1099	35.13	1.1758	1089242	0.0087	3215	2.706E-06	8.23	
801	27.57	0.9826	723831	0.0089	35807	2.494E-07	5.08	1107	35.33	1.1800	1090616	0.0087	3031	2.903E-06	8.32	
807	27.73	0.9872	741895	0.0090	35028	2.572E-07	5.14	1114	35.53	1.1845	1092252	0.0087	2899	3.052E-06	8.41	
813	27.88	0.9916	758859	0.0089	33811	2.630E-07	5.20	1123	35.73	1.1888	1093714	0.0091	2993	3.201E-06	8.51	
819	28.03	0.9961	775705	0.0091	33723	2.705E-07	5.25	1131	35.96	1.1937	1095245	0.0094	2899	3.239E-06	8.61	
	28.19	1.0007	792582					1139	36.17	1.1982	1096613	0.0088	2599	3.394E-06	8.70	
	28.34	1.0049	808585					1147	36.37	1.2025	1097844	0.0088	2477	3.562E-06	8.80	
837	28.49	1.0093	824320	0.0089	31332	2.841E-07	5.43	1156	36.59	1.2070	1099091	0.0093	2342	3.677E-06	8.90	
843	28.65	1.0138	839917	0.0094	31185	3.000E-07	5.49	1164	36.82	1.2118	1100387	0.0092	2242	3.777E-06	9.00	
849	28.82	1.0187	855505	0.0094	30476	3.071E-07	5.56	1173	37.03	1.2162	1101533	0.0089	2193	4.079E-06	9.11	
856	28.98	1.0232	870392	0.0089	28439	3.121E-07	5.62	1181	37.25	1.2208	1102580	0.0089	2094	4.234E-06	9.21	
862	29.14	1.0275	883944	0.0088	27058	3.258E-07	5.68		37.47	1.2251	1103627					
868	29.30	1.0320	897450	0.0090	27034	3.323E-07	5.75		37.69	1.2297	1104724					
875	29.46	1.0365	910978	0.0089	27019	3.304E-07	5.81	1208	37.91	1.2341	1105772	0.0094	2046	4.583E-06	9.53	
881	29.62	1.0409	924470	0.0087	23027	3.759E-07	5.88	1216	38.16	1.2390	1106770	0.0093	1898	4.924E-06	9.64	
	29.78	1.0452	934006					1225	38.38	1.2434	1107670	0.0086	1743	4.903E-06	9.75	
	29.99	1.0509	940920					1234	38.60	1.2476	1108559	0.0086	1743	4.903E-06	9.85	
902	30.12	1.0542	950546	0.0079	21063	3.731E-07	6.09	1242	38.82	1.2520	1109414	0.0088	1628	5.395E-06	9.96	
907	30.29	1.0588	961982	0.0090	23286	3.864E-07	6.14	1251	39.05	1.2564	1110187	0.0090	1587	5.644E-06	10.07	
914	30.46	1.0632	973833	0.0091	23266	3.910E-07	6.22	1261	39.29	1.2609	1111001	0.0093	1467	5.606E-06	10.19	
921	30.63	1.0679	985248	0.0090	22506	4.191E-07	6.28	1270	39.53	1.2657	1111855	0.0094	1368	5.639E-06	10.31	
928	30.80	1.0723	995339	0.0089	19742	4.499E-07	6.36	1279	39.78	1.2703	1112669	0.0087	1327	5.731E-06	10.42	
								1288	40.00	1.2744	1113381	0.0086	1204	6.100E-06	10.54	
								1297	40.24	1.2789	1114072	0.0091	1083	6.545E-06	10.65	
								1307	40.49	1.2835	1114764	0.0093	1053	6.884E-06	10.78	
								1316	40.75	1.2882	1115426	0.0092	1008	7.057E-06	10.90	
								1326	40.99	1.2927	1116072	0.0089	954	7.325E-06	11.03	



TABLE I32 (Continued)

Specimen Id. FZGL18				Page 3				Specimen Id. FZGL18				Page 4			
Pinch (lbs)	EAB/P (in)	N (X1)	As (in)	AN (X1)	AB/AN (in/cyc)	AK (ksi/in)	Pinch (lbs)	EAB/P (in)	N (X1)	As (in)	AN (X1)	AB/AN (in/cyc)	AK (ksi/in)		
1335	41.24	1116639	0.0088	1062	8.264E-06	11.15	2126	64.77	1.6080	1141807	0.0087	7.129E-05	24.24		
1344	41.48	1117134	0.0088	1016	8.630E-06	11.27	2140	65.20	1.6121	1141868	0.0089	7.340E-05	24.53		
1354	41.73	1117655	0.0096	1146	8.337E-06	11.41	2151	65.69	1.6169	1141928	0.0086	7.418E-05	24.77		
1364	42.02	1118280	0.0097	1147	8.426E-06	11.54	2166	66.09	1.6206	1141983	0.0090	8.211E-05	25.08		
1373	42.28	1118802	0.0080	985	8.106E-06	11.66	2179	66.64	1.6259	1142038	0.0099	9.042E-05	25.35		
1383	42.48	1119265	0.0081	995	8.150E-06	11.79	2193	67.13	1.6305	1142092	0.0092	8.442E-05	25.66		
1392	42.75	1119797	0.0094	1041	9.059E-06	11.92	2207	67.62	1.6351	1142147	0.0091	8.327E-05	25.95		
1402	43.03	1120306	0.0091	997	9.147E-06	12.05	2221	68.12	1.6396	1142201	0.0092	8.923E-05	26.25		
1412	43.29	1120794	0.0088	932	9.416E-06	12.19	2235	68.63	1.6442	1142250	0.0091	9.442E-05	26.55		
1422	43.55	1121238	0.0085	887	9.553E-06	12.32	2249	69.13	1.6487	1142298	0.0093	9.656E-05	26.87		
1432	43.79	1121681	0.0091	951	9.580E-06	12.47	2262	69.67	1.6536	1142346	0.0091	1.006E-04	27.16		
1442	44.10	1122189	0.0095	974	9.768E-06	12.60	2276	70.15	1.6578	1142398	0.0085	1.017E-04	27.47		
1453	44.37	1122655	0.0092	921	9.992E-06	12.76	2290	70.65	1.6621	1142430	0.0090	1.070E-04	27.78		
1463	44.67	1123110	0.0093	888	1.052E-05	12.90	2303	71.19	1.6668	1142472	0.0092	1.092E-04	28.09		
1473	44.95	1123543	0.0085	804	1.051E-05	13.04	2318	71.71	1.6713	1142514	0.0097	1.153E-04	28.44		
1484	45.19	1123914	0.0086	794	1.085E-05	13.19	2332	72.33	1.6764	1142556	0.0098	1.271E-04	28.76		
1494	45.49	1124337	0.0095	853	1.116E-05	13.34	2347	72.88	1.6811	1142591	0.0089	1.365E-04	29.10		
1504	45.79	1124767	0.0088	772	1.141E-05	13.48	2360	73.39	1.6853	1142621	0.0082	1.398E-04	29.42		
1514	46.05	1125109	0.0082	689	1.186E-05	13.63	2375	73.89	1.6893	1142650	0.0093	1.594E-04	29.77		
1525	46.32	1125456	0.0095	774	1.233E-05	13.80	2389	74.54	1.6946	1142679	0.0102	1.746E-04	30.11		
1536	46.67	1125883	0.0100	805	1.243E-05	13.95	2405	75.16	1.6996	1142709	0.0096	1.622E-04	30.48		
1547	46.97	1126261	0.0090	702	1.270E-05	14.12	2420	75.74	1.7042	1142738	0.0093	1.594E-04	30.85		
1558	47.26	1126585	0.0085	646	1.320E-05	14.27	2434	76.35	1.7089	1142767	0.0089	1.730E-04	31.19		
1568	47.54	1126907	0.0084	631	1.331E-05	14.43	2447	76.89	1.7131	1142790	0.0082	1.776E-04	31.54		
1579	47.83	1127216	0.0088	619	1.421E-05	14.59	2461	77.42	1.7171	1142814	0.0085	1.831E-04	31.88		
1590	48.14	1127526	0.0094	606	1.558E-05	14.75	2475	78.00	1.7216	1142836	0.0095	1.932E-04	32.25		
							2492	78.68	1.7267	1142863	0.0107	2.086E-04	32.66		
1808	54.57	1139298	0.0088	342	2.569E-05	18.28	2508	79.45	1.7323	1142888	0.0110	2.453E-04	33.09		
1822	54.86	1139445	0.0085	305	2.796E-05	18.51	2522	80.18	1.7377	1142908	0.0086	2.088E-04	33.45		
1833	55.26	1139603	0.0096	318	3.010E-05	18.71	2537	80.62	1.7409	1142929	0.0073	1.942E-04	33.85		
1846	55.65	1139762	0.0093	279	3.318E-05	18.93	2551	81.19	1.7450	1142946	0.0096	2.204E-04	34.22		
							2568	81.97	1.7505	1142972	0.0118	2.146E-04	34.67		
							2582	82.88	1.7568	1143001	0.0100	2.228E-04	35.07		
1915	56.42	1139993	0.0314	862	3.644E-05	20.15	2602	83.42	1.7605	1143017	0.0094	2.582E-04	35.60		
1928	56.87	1140101	0.0302	934	3.619E-05	20.39	2614	84.25	1.7662	1143037	0.0099	2.476E-04	35.96		
1971	59.16	1140854	0.0096	173	5.574E-05	21.21	2635	84.88	1.7704	1143057	0.0110	2.743E-04	36.52		
1983	59.53	1140935	0.0093	166	5.623E-05	21.42	2649	85.90	1.7772	1143077	0.0116	2.905E-04	36.94		
2000	60.39	1141027	0.0104	192	5.400E-05	21.74	2675	86.64	1.7820	1143097	0.0139	3.485E-04	37.68		
2011	61.00	1141101	0.0106	193	5.469E-05	21.96	2702	88.06	1.7911	1143117	0.0209	4.708E-04	38.48		
2024	61.38	1141220	0.0067	123	5.469E-05	22.21									
2036	61.64	1141343	0.0074	122	6.028E-05	22.45									
2048	62.08	1141416	0.0097	147	6.621E-05	22.68									
2060	62.57	1141490	0.0091	134	6.817E-05	22.92									
2074	62.97	1141550	0.0085	128	6.632E-05	23.20									
2087	63.41	1141618	0.0090	134	6.704E-05	23.45									
2100	63.86	1141685	0.0090	128	7.016E-05	23.71									
2113	64.31	1141746	0.0090	122	7.355E-05	23.98									

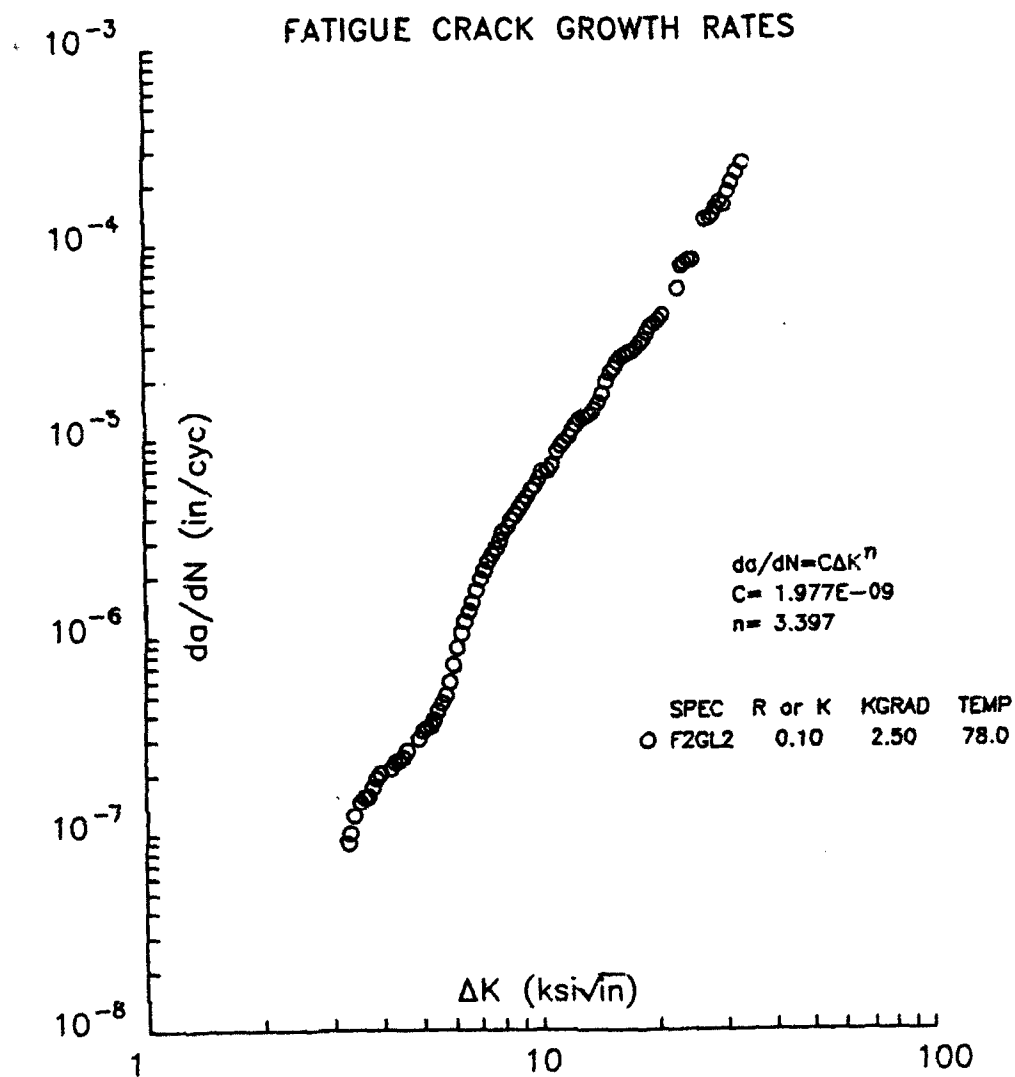


Figure I10. Fatigue Crack Growth Rate Data for 2095-T8 0.5 Inch Thick Plate (L-T orientation, KGRAD 2.50). Northrop.

TABLE I33

Fatigue Crack Growth Data Associated with Figure I10 (Specimen F2GL2)

AUTOMATED FATIGUE CRACK  
GROWTH RATE ANALYSIS

Specimen Id.	F2GL2	Geometry	C(T)
Contract #	WB02115.1	Orientation	L-T
Material	WELDALITE	Yield (ksi)	101.0
Temperature (F)	78	Modulus	10.6
Environment	Lab. air		

## Specimen Dimensions (in)

Thickness	0.495	Notch depth	0.605
Width	2.996	Gage length	1.000
Height	3.600	Alpha ratio	1.250

## Pretcrack Parameters

Pmax (lbs)	911.0	Stress ratio (R)	0.10
Final a (in)	0.680	Kmax	4.91

## Test Parameters

Initial a (in)	0.771	Initial K	3.40
K-gradient	2.50	Stress ratio (R)	0.10

K Coeff	EvB/P Coeff	Analysis Codes
0.886000	1.000980	KRP      1    0
4.640000	-4.669510	
-13.320000	18.460100	
14.720000	-236.824997	
-5.600000	1214.880000	
0.000000	-2143.570100	

## Visual Observations

EvB/P	Crack (EvB/P)	Crack (visual)	Error	CAF
24.03	0.855	0.849	-.006	0.985
25.57	0.909	0.910	0.002	0.986
27.48	0.970	0.972	0.002	0.988
30.72	1.063	1.069	0.007	0.991
32.46	1.108	1.110	0.002	0.993
34.22	1.150	1.150	-.000	0.994
36.98	1.211	1.206	-.006	0.996

## Comments

Date of test: 01-28-1992

TABLE I33 (Continued)

Specimen Id. F20L2				Page 1				Specimen Id. F20L2				Page 2			
Peak (lbs)	E4B/P (in)	N (X1)	A <sub>0</sub> (in)	ΔN (X1)	Δa/ΔN (in/cyc)	ΔK (ksi/in)	Peak (lbs)	E4B/P (in)	N (X1)	A <sub>0</sub> (in)	ΔN (X1)	Δa/ΔN (in/cyc)	ΔK (ksi/in)		
605	21.89	0.7752	0.0177	174177	9.074E-08	3.23	1309	40.08	1.2723	0.0271	3596	7.333E-06	10.65		
614	22.12	0.7841	0.0181	271818	1.019E-07	3.31	1337	40.56	1.2812	0.0172	1986	8.666E-06	11.01		
623	22.35	0.7933	0.0185	373258	1.258E-07	3.38	1356	41.02	1.2895	0.0177	1906	9.275E-06	11.26		
632	22.64	0.8118	0.0181	520772	1.457E-07	3.46	1375	41.54	1.2988	0.0181	1846	9.793E-06	11.50		
642	23.08	0.8207	0.0178	577362	1.538E-07	3.54	1395	42.03	1.3076	0.0181	1761	1.030E-05	11.77		
651	23.32	0.8296	0.0184	636611	1.566E-07	3.62	1415	42.57	1.3170	0.0186	1682	1.106E-05	12.04		
661	23.58	0.8391	0.0185	694873	1.736E-07	3.70	1435	43.11	1.3262	0.0178	1499	1.190E-05	12.31		
671	23.83	0.8481	0.0182	743019	1.936E-07	3.79	1455	43.62	1.3348	0.0169	1336	1.266E-05	12.59		
681	24.09	0.8573	0.0183	788603	2.043E-07	3.88	1475	44.12	1.3431	0.0174	1348	1.288E-05	12.87		
	24.35	0.8665		832847			1496	44.68	1.3522	0.0188	1413	1.332E-05	13.16		
	24.60	0.8752		882227			1517	45.29	1.3619	0.0187	1384	1.351E-05	13.46		
711	24.88	0.8853	0.0196	930654	2.163E-07	4.15	1539	45.85	1.3709	0.0179	1261	1.423E-05	13.78		
723	25.16	0.8949	0.0191	973001	2.320E-07	4.25	1561	46.43	1.3799	0.0181	1168	1.553E-05	14.09		
733	25.44	0.9044	0.0185	1013179	2.371E-07	4.35	1583	47.03	1.3890	0.0179	1061	1.713E-05	14.41		
744	25.71	0.9133	0.0180	1050922	2.455E-07	4.45	1605	47.62	1.3978	0.0179	901	1.981E-05	14.74		
755	25.98	0.9224	0.0185	1086482	2.663E-07	4.55	1626	48.23	1.4069	0.0177	805	2.204E-05	15.07		
	26.27	0.9318		1120360			1648	48.83	1.4156	0.0172	740	2.323E-05	15.40		
	26.51	0.9395		1163004			1671	49.42	1.4240	0.0181	720	2.509E-05	15.76		
789	26.87	0.9509	0.0204	1202178	3.074E-07	4.86	1693	50.10	1.4336	0.0184	698	2.643E-05	16.10		
801	27.15	0.9599	0.0179	1229428	3.365E-07	4.99	1717	50.75	1.4425	0.0180	661	2.721E-05	16.48		
813	27.44	0.9688	0.0180	1255395	3.502E-07	5.10	1741	51.42	1.4516	0.0183	649	2.815E-05	16.86		
825	27.74	0.9779	0.0182	1280840	3.594E-07	5.21	1764	52.11	1.4608	0.0181	636	2.846E-05	17.24		
837	28.04	0.9870	0.0184	1305921	3.814E-07	5.33	1789	52.79	1.4698	0.0181	610	2.962E-05	17.64		
850	28.35	0.9963	0.0191	1329194	4.255E-07	5.46	1812	53.50	1.4788	0.0174	559	3.119E-05	18.02		
862	28.69	1.0061	0.0189	1350893	4.684E-07	5.58	1836	54.16	1.4871	0.0173	534	3.231E-05	18.43		
876	29.00	1.0152	0.0182	1369471	5.150E-07	5.71	1861	54.88	1.4961	0.0190	547	3.484E-05	18.86		
889	29.32	1.0243	0.0185	1386136	5.991E-07	5.84	1886	55.71	1.5062	0.0193	508	3.800E-05	19.29		
902	29.66	1.0337	0.0187	1400416	7.272E-07	5.98	1912	56.47	1.5154	0.0180	457	3.944E-05	19.75		
915	29.99	1.0430	0.0186	1411834	8.866E-07	6.12	1938	57.23	1.5242	0.0180	444	4.056E-05	20.21		
929	30.33	1.0523	0.0184	1421403	1.041E-06	6.26	1964	58.02	1.5334	0.0186	431	4.310E-05	20.68		
943	30.67	1.0614	0.0182	1429512	1.202E-06	6.40		58.86	1.5428						
956	31.01	1.0705	0.0180	1436555	1.351E-06	6.54		60.45	1.5603						
970	31.35	1.0794	0.0179	1442851	1.496E-06	6.69	2068	61.43	1.5707	0.0185	312	5.938E-05	22.62		
985	31.70	1.0885	0.0185	1448534	1.729E-06	6.84	2096	62.20	1.5789	0.0169	218	7.773E-05	23.17		
999	32.07	1.0979	0.0185	1453526	1.955E-06	7.00	2121	63.06	1.5876	0.0175	218	8.041E-05	23.66		
1014	32.43	1.1070	0.0187	1458010	2.167E-06	7.16	2147	63.92	1.5963	0.0179	217	8.238E-05	24.20		
1029	32.82	1.1166	0.0186	1462165	2.412E-06	7.32	2175	64.85	1.6055	0.0190	230	8.254E-05	24.77		
1044	33.19	1.1256	0.0181	1465721	2.620E-06	7.49		65.87	1.6153						
1060	33.56	1.1346	0.0187	1469055	2.813E-06	7.67		66.92	1.6253						
1076	33.97	1.1433	0.0191	1472369	3.092E-06	7.84	2265	68.57	1.6405	0.0202	152	1.331E-04	26.66		
1091	34.37	1.1537	0.0179	1475234	3.379E-06	8.02	2302	69.12	1.6455	0.0137	100	1.372E-04	27.47		
1108	34.74	1.1622	0.0181	1477655	3.627E-06	8.21	2325	70.11	1.6543	0.0183	129	1.413E-04	27.97		
1124	35.17	1.1719	0.0192	1480232	3.916E-06	8.39	2352	71.20	1.6638	0.0184	120	1.538E-04	28.60		
1140	35.59	1.1814	0.0183	1482565	4.182E-06	8.59	2381	72.25	1.6727	0.0181	109	1.652E-04	29.27		
1157	35.99	1.1902	0.0179	1484611	4.450E-06	8.79	2409	73.35	1.6818	0.0177	111	1.594E-04	29.92		
1174	36.41	1.1993	0.0183	1486586	4.794E-06	8.98	2437	74.40	1.6904	0.0171	93	1.848E-04	30.58		
1191	36.84	1.2085	0.0183	1488434	5.157E-06	9.19	2471	75.47	1.6990	0.0209	101	2.070E-04	31.39		
1208	37.28	1.2176	0.0181	1490136	5.539E-06	9.40	2511	77.06	1.7113	0.0289	123	2.346E-04	32.40		
1226	37.72	1.2266	0.0180	1491705	5.870E-06	9.61		79.25	1.7278						
1244	38.17	1.2356	0.0185	1493203	6.339E-06	9.84	2550	80.83	1.7393						
1262	38.66	1.2452	0.0185	1494628	6.881E-06	10.05		82.87	1.7538						
1291	39.12	1.2540	0.0272	1495886	6.919E-06	10.42		85.09	1.7689						

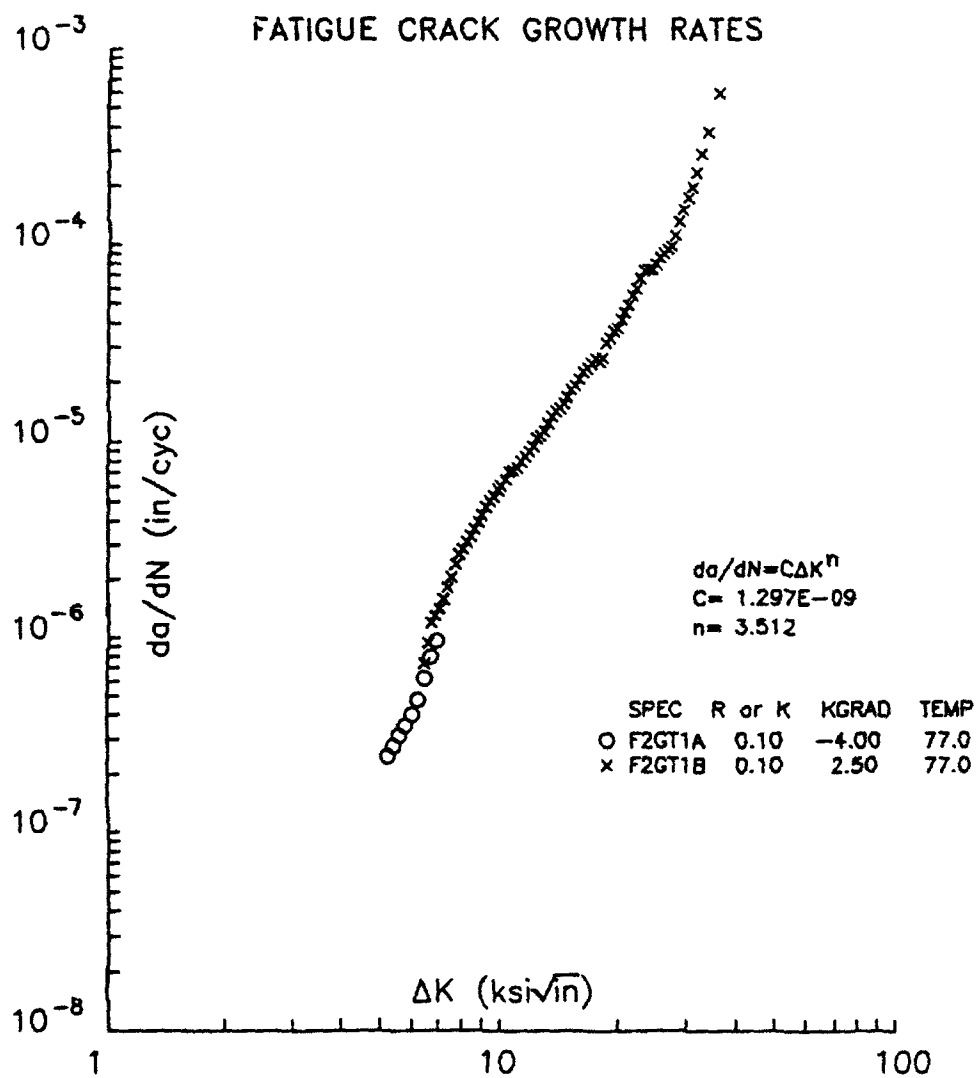


Figure I11. Fatigue Crack Growth Rate Data for 2095-T8 0.5 Inch Thick Plate (T-L orientation, KGRAD - 4.00 and 2.50). Northrop.

TABLE I34

Fatigue Crack Growth Data Associated with Figure I11 (Specimen F2GT1A)

AUTOMATED FATIGUE CRACK  
GROWTH RATE ANALYSIS

Specimen Id.	F2GT1A	Geometry	C(T)
Contract #	WB02115N	Orientation	T-L
Material	WELDALITE	Yield (ksi)	51.0
Temperature (F)	77	Modulus	10.9
Environment	Lab. air		

## Specimen Dimensions (in)

Thickness	0.486	Notch depth	0.614
Width	2.997	Gage length	1.000
Height	3.600	Alpha ratio	1.250

## Precrack Parameters

Pmax (lbs)	1271.0	Stress ratio (R)	0.10
Final a (in)	0.901	Kmax	8.50

## Test Parameters

Initial a (in)	0.901	Initial K	8.50
K-gradient	-4.00	Stress ratio (R)	0.10

K Coeff	EvB/P Coeff	Analysis Codes
0.886000	1.000980	KRP 2 0
4.640000	-4.669510	
-13.320000	18.460100	
14.720000	-236.824997	
-5.600000	1214.880000	
0.000000	-2143.570100	

## Visual Observations

EvB/P	Crack (EvB/P)	Crack (visual)	Error	CAF
24.97	0.900	0.872	-.028	1.000
26.23	0.941	0.947	0.005	1.000
28.03	0.996	1.010	0.014	1.000
32.61	1.118	1.119	0.001	1.000
37.42	1.224	1.203	-.021	1.000
40.54	1.285	1.261	-.024	1.000
47.82	1.405	1.381	-.024	1.000
50.85	1.447	1.426	-.022	1.000
55.56	1.508	1.481	-.027	1.000
58.77	1.545	1.525	-.020	1.000

Pmax (lbs)	EvB/P	a (in)	N (X1)	Δa (in)	ΔN (X1)	Δa/ΔN (in/cyc)	ΔK (ksi/in)
	25.44	0.9161	12656				
1127	25.73	0.9256	21925	0.0183	18984	9.616E-07	6.93
1078	26.00	0.9343	31640	0.0174	21722	8.018E-07	6.68
1033	26.27	0.9430	43646	0.0174	28109	6.203E-07	6.45
989	26.55	0.9518	59749	0.0179	37173	4.808E-07	6.22
947	26.85	0.9609	80820	0.0183	45759	3.998E-07	6.01
906	27.15	0.9701	105508	0.0185	52122	3.552E-07	5.79
867	27.46	0.9794	132941	0.0183	57804	3.164E-07	5.58
829	27.76	0.9884	163312	0.0178	64272	2.772E-07	5.38
794	28.06	0.9972	197213	0.0178	71996	2.477E-07	5.19
	28.37	1.0062	235308				

TABLE I35

Fatigue Crack Growth Data Associated with Figure I11 (Specimen F2GT1B)

AUTOMATED FATIGUE CRACK  
GROWTH RATE ANALYSIS

Specimen Id.	F2GT1B	Geometry	C(T)
Contract #	WB02115N	Orientation	T-L
Material	WELDALITE	Yield (ksi)	101.0
Temperature (F)	77	Modulus	10.9
Environment	Lab. air		

## Specimen Dimensions (in)

Thickness	0.486	Notch depth	0.614
Width	2.997	Gage length	0.200
Height	3.600	Alpha ratio	1.000

## Precrack Parameters

Pmax (lbs)	1271.0	Stress ratio (R)	0.10
Final a (in)	0.901	Kmax	8.50

## Test Parameters

Initial a (in)	1.064	Initial K	4.40
K-gradient	2.50	Stress ratio (R)	0.10

K Coeff	EvB/P Coeff	Analysis Codes
0.886000	1.000980	KRP 2 0
4.640000	-4.669510	
-13.320000	18.460100	
14.720000	-236.824997	
-5.600000	1214.880000	
0.000000	-2143.570100	

## Visual Observations

EvB/P	Crack (EvB/P)	Crack (visual)	Error	CAF
24.97	0.900	0.872	-.028	1.000
26.23	0.941	0.947	0.005	1.000
28.03	0.996	1.010	0.014	1.000
32.61	1.118	1.119	0.001	1.000
37.42	1.224	1.203	-.021	1.000
40.54	1.285	1.261	-.024	1.000
47.82	1.405	1.381	-.024	1.000
50.85	1.447	1.426	-.022	1.000
55.56	1.508	1.481	-.027	1.000
58.77	1.545	1.525	-.020	1.000

## Comments

Date of test: 01-14-1992

TABLE I35 (Continued)

Specimen Id. F2GT18										Page 1		Specimen Id. F2GT18										Page 2	
Peak (lbs)	EAB/P (in)	M (X1)	Aa (in)	AN (X1)	AB/AN (in/cyc)	AK (ksi/in)	Peak (lbs)	EAB/P (in)	M (X1)	Aa (in)	AN (X1)	AB/AN (in/cyc)	AK (ksi/in)	Peak (lbs)	EAB/P (in)	M (X1)	Aa (in)	AN (X1)	AB/AN (in/cyc)	AK (ksi/in)			
784	38.67	1.2491	493512	24618	7.364E-07	6.43	1483	74.00	1.6905	0.0185	548	3.362E-05	18.93	784	38.67	1.2491	493512	24618	7.364E-07	6.43			
795	39.13	1.2582	506627	19751	9.345E-07	6.58	1502	75.09	1.6992	0.0178	484	3.675E-05	19.38	795	39.61	1.2673	518130	0.0185	19751	9.345E-07	6.58		
806	40.11	1.2673	518130	15063	1.195E-06	6.73	1518	76.24	1.7083	0.0174	459	3.726E-05	19.80	806	40.58	1.2766	526378	0.0180	15063	1.195E-06	6.73		
818	40.58	1.2766	526378	13111	1.305E-06	6.88	1536	77.31	1.7166	0.0169	402	4.174E-05	20.24	818	41.04	1.2853	533193	0.0171	13111	1.305E-06	6.88		
830	41.04	1.2853	533193	12495	1.413E-06	7.04	1552	78.45	1.7251	0.0166	362	4.587E-05	20.66	830	41.55	1.2938	539489	0.0177	12495	1.413E-06	7.04		
842	41.55	1.2938	539489	11807	1.579E-06	7.20	1571	79.53	1.7332	0.0192	386	4.940E-05	21.17	842	42.09	1.3029	545688	0.0186	11807	1.579E-06	7.20		
854	42.09	1.3029	545688	10345	1.819E-06	7.36	1589	81.07	1.7443	0.0202	364	5.554E-05	21.63	854	42.63	1.3124	551296	0.0188	10345	1.819E-06	7.36		
866	42.63	1.3124	551296	8543	2.059E-06	7.53	1609	82.36	1.7534	0.0183	303	6.054E-05	22.19	866	43.11	1.3217	556032	0.0176	8543	2.059E-06	7.53		
879	43.11	1.3217	556032	7405	2.422E-06	7.71	1628	83.70	1.7627	0.0189	277	6.804E-05	22.72	879	43.69	1.3300	559839	0.0179	7405	2.422E-06	7.71		
890	43.69	1.3300	559839	6559	2.717E-06	7.87	1645	85.13	1.7723	0.0179	240	7.448E-05	23.22	890	44.18	1.3396	563437	0.0178	6559	2.717E-06	7.87		
903	44.18	1.3396	563437	6017	2.876E-06	8.06	1664	86.38	1.7806	0.0172	228	7.550E-05	23.76	903	44.74	1.3478	566945	0.0173	6017	2.876E-06	8.06		
916	44.74	1.3478	566945	5983	3.105E-06	8.24	1682	87.77	1.7895	0.0182	240	7.550E-05	24.29	916	45.33	1.3569	569454	0.0186	5983	3.105E-06	8.24		
929	45.33	1.3569	569454	5491	3.334E-06	8.42	1700	89.23	1.7987	0.0181	228	7.550E-05	24.84	929	45.90	1.3664	572381	0.0183	5491	3.334E-06	8.42		
942	45.90	1.3664	572381	4884	3.626E-06	8.62	1719	90.68	1.8077	0.0186	216	8.555E-05	25.43	942	46.47	1.3752	574945	0.0177	4884	3.626E-06	8.62		
955	46.47	1.3752	574945	4461	3.954E-06	8.81	1738	92.29	1.8173	0.0196	203	9.553E-05	26.04	955	47.04	1.3841	577265	0.0176	4461	3.954E-06	8.81		
968	47.04	1.3841	577265	4126	4.271E-06	9.01	1757	93.98	1.8272	0.0193	178	9.553E-05	26.66	968	47.63	1.3929	579406	0.0176	4126	4.271E-06	9.01		
982	47.63	1.3929	579406	3816	4.681E-06	9.21	1776	95.63	1.8366	0.0176	166	1.166E-04	27.27	982	48.24	1.4017	581391	0.0179	3816	4.681E-06	9.21		
995	48.24	1.4017	581391	3564	4.994E-06	9.42	1796	97.09	1.8448	0.0185	153	1.166E-04	27.95	995	48.85	1.4107	583221	0.0178	3564	4.994E-06	9.42		
1009	48.85	1.4107	583221	3442	5.323E-06	9.64	1814	99.00	1.8551	0.0201	133	1.166E-04	28.59	1009	49.52	1.4195	584955	0.0183	3442	5.323E-06	9.64		
1022	49.52	1.4195	584955	2967	5.790E-06	9.84	1835	100.84	1.8649	0.0202	116	1.166E-04	29.34	1022	50.07	1.4291	586663	0.0172	2967	5.790E-06	9.84		
1036	50.07	1.4291	586663	2739	6.013E-06	10.07	1855	102.87	1.8753	0.0203	91	1.166E-04	30.07	1036	50.71	1.4367	587922	0.0165	2739	6.013E-06	10.07		
1051	50.71	1.4367	587922	3050	6.479E-06	10.30	1874	104.84	1.8852	0.0196	81	1.166E-04	30.78	1051	51.51	1.4455	589072	0.0198	3050	6.479E-06	10.30		
1064	51.51	1.4455	589072	2701	7.150E-06	10.53	1895	106.49	1.8932	0.0191	88	1.166E-04	31.59	1064	52.14	1.4545	590972	0.0193	2701	7.150E-06	10.53		
1080	52.14	1.4545	590972	2339	7.215E-06	10.78	1918	108.82	1.9043	0.0260	88	2.565E-04	32.51	1080	52.79	1.4648	592103	0.0169	2339	7.215E-06	10.78		
1095	52.79	1.4648	592103	2491	7.466E-06	11.04	1949	112.09	1.9192	0.0345	91	3.510E-04	33.78	1095	53.58	1.4734	593311	0.0186	2491	7.466E-06	11.04		
1109	53.58	1.4734	593311	2319	7.986E-06	11.27	2004	116.58	1.9388	0.0579	96	6.130E-04	36.14	1109	54.25	1.4834	594594	0.0185	2319	7.986E-06	11.27		
1125	54.25	1.4834	594594	2075	8.472E-06	11.55								1125	54.99	1.4919	595631	0.0176	2075	8.472E-06	11.55		
1139	54.99	1.4919	595631	2031	8.943E-06	11.80								1139	55.73	1.5010	596669	0.0182	2031	8.943E-06	11.80		
1154	55.73	1.5010	596669	1807	9.508E-06	12.06								1154	56.42	1.5100	597662	0.0172	1807	9.508E-06	12.06		
1170	56.42	1.5100	597662	1695	1.042E-05	12.34								1170	57.22	1.5182	598476	0.0177	1695	1.042E-05	12.34		
1184	57.22	1.5182	598476	1681	1.079E-05	12.60								1184	57.98	1.5277	599357	0.0181	1681	1.079E-05	12.60		
1200	57.98	1.5277	599357	1573	1.138E-05	12.90								1200	58.79	1.5363	600157	0.0179	1573	1.138E-05	12.90		
1216	58.79	1.5363	600157	1489	1.250E-05	13.20								1216	59.64	1.5456	600930	0.0186	1489	1.250E-05	13.20		
1232	59.64	1.5456	600930	1375	1.341E-05	13.50								1232	59.64	1.5550	601647	0.0185	1375	1.341E-05	13.50		
1248	60.48	1.5550	601647	1275	1.422E-05	13.82								1248	60.48	1.5641	602305	0.0181	1275	1.422E-05	13.82		
1264	61.32	1.5641	602305	1162	1.482E-05	14.12								1264	61.32	1.5731	602921	0.0172	1162	1.482E-05	14.12		
1281	62.11	1.5731	602921	1136	1.570E-05	14.45								1281	62.11	1.5813	603467	0.0178	1136	1.570E-05	14.45		
1296	63.04	1.5813	603467	1082	1.681E-05	14.76								1296	63.04	1.5909	604057	0.0182	1082	1.681E-05	14.76		
1313	63.90	1.5909	604057	980	1.845E-05	15.12								1313	63.90	1.5995	604549	0.0181	980	1.845E-05	15.12		
1329	64.86	1.5995	604549	931	1.943E-05	15.45								1329	64.86	1.6090	605036	0.0181	931	1.943E-05	15.45		
1346	65.75	1.6090	605036	867	2.070E-05	15.81								1346	65.75	1.6176	605480	0.0179	867	2.070E-05	15.81		
1363	66.73	1.6176	605480	828	2.256E-05	16.17								1363	66.73	1.6269	605903	0.0187	828	2.256E-05	16.17		
1380	67.73	1.6269	605903	760	2.367E-05	16.54								1380	67.73	1.6363	606308	0.0180	760	2.367E-05	16.54		
1397	68.68	1.6363	606308	712	2.496E-05	16.93								1397	68.68	1.6449	606663	0.0178	712	2.496E-05	16.93		
1414	69.71	1.6449	606663	669	2.651E-05	17.29								1414	69.71	1.6541	607021	0.0177	669	2.651E-05	17.29		
1432	70.69	1.6541	607021	709	2.556E-05	17.70								1432	70.69	1.6627	607332	0.0181	709	2.556E-05	17.70		
1448	71.80	1.6627	607332	670	2.692E-05	18.08								1448	71.80	1.6722	607730	0.0180	670	2.692E-05	18.08		
1467	72.81	1.6722	607730	573	3.185E-05	18.53								1467	72.81	1.6807	608001	0.0183	573	3.185E-05	18.53		



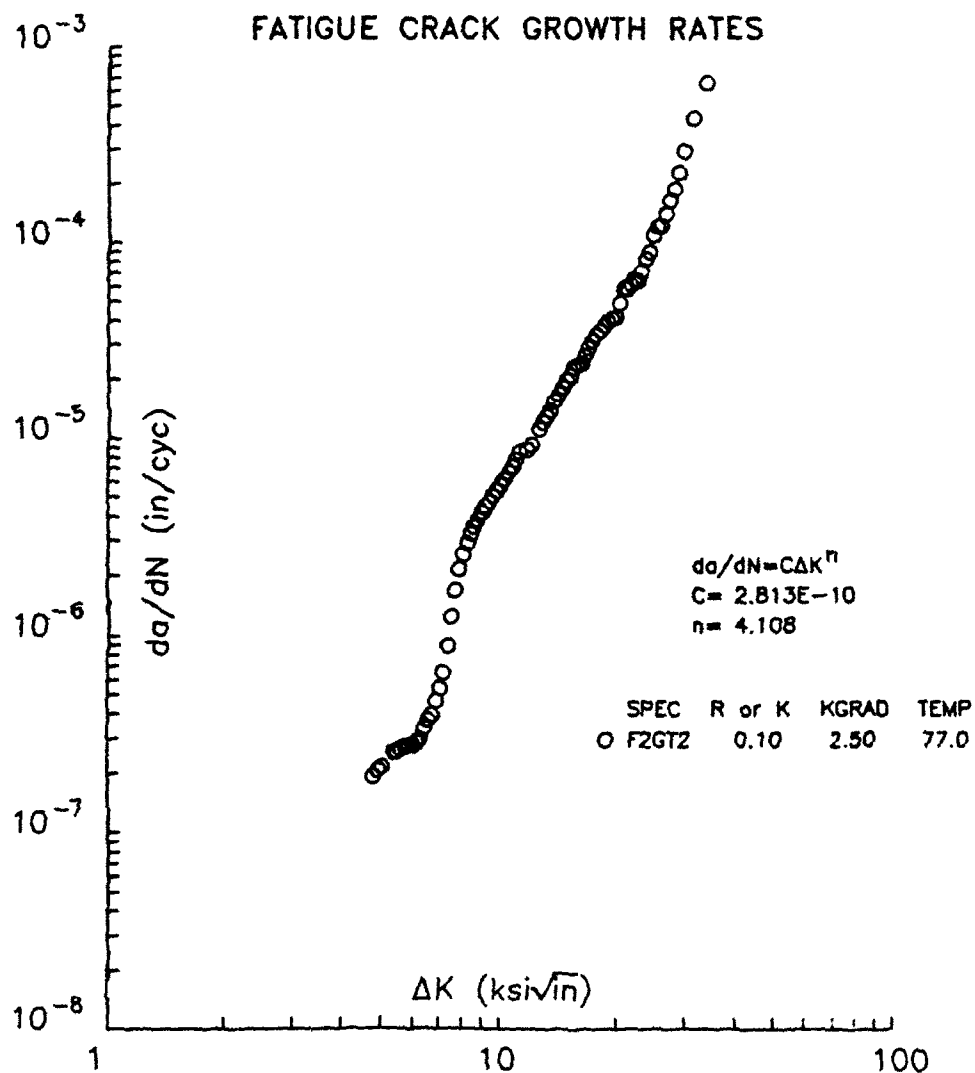


Figure I12. Fatigue Crack Growth Rate Data for 2095-T8 0.5 Inch Thick Plate (T-L orientation, KGRAD 2.50). Northrop.

TABLE I36

Fatigue Crack Growth Data Associated with Figure I12 (Specimen F2GT2)

AUTOMATED FATIGUE CRACK  
GROWTH RATE ANALYSIS

Specimen Id.	F2GT2	Geometry	C(T)
Contract #	WB02115N	Orientation	T-L
Material	WELDALITE	Yield (ksi)	101.0
Temperature (F)	77	Modulus	10.8
Environment	Lab. air		

## Specimen Dimensions (in)

Thickness	0.494	Notch depth	0.605
Width	2.999	Gage length	0.200
Height	3.600	Alpha ratio	1.000

## Precrack Parameters

Pmax (lbs)	1166.0	Stress ratio (R)	0.10
Final a (in)	0.665	Kmax	6.21

## Test Parameters

Initial a (in)	0.741	Initial K	4.60
K-gradient	2.50	Stress ratio (R)	0.10

K Coeff	EvB/P Coeff	Analysis Codes
0.886000	1.000980	KRP 1 0
4.640000	-4.569510	
-13.320000	18.460100	
14.720000	-236.824997	
-5.600000	1214.880000	
0.000000	-2143.570100	

## Visual Observations

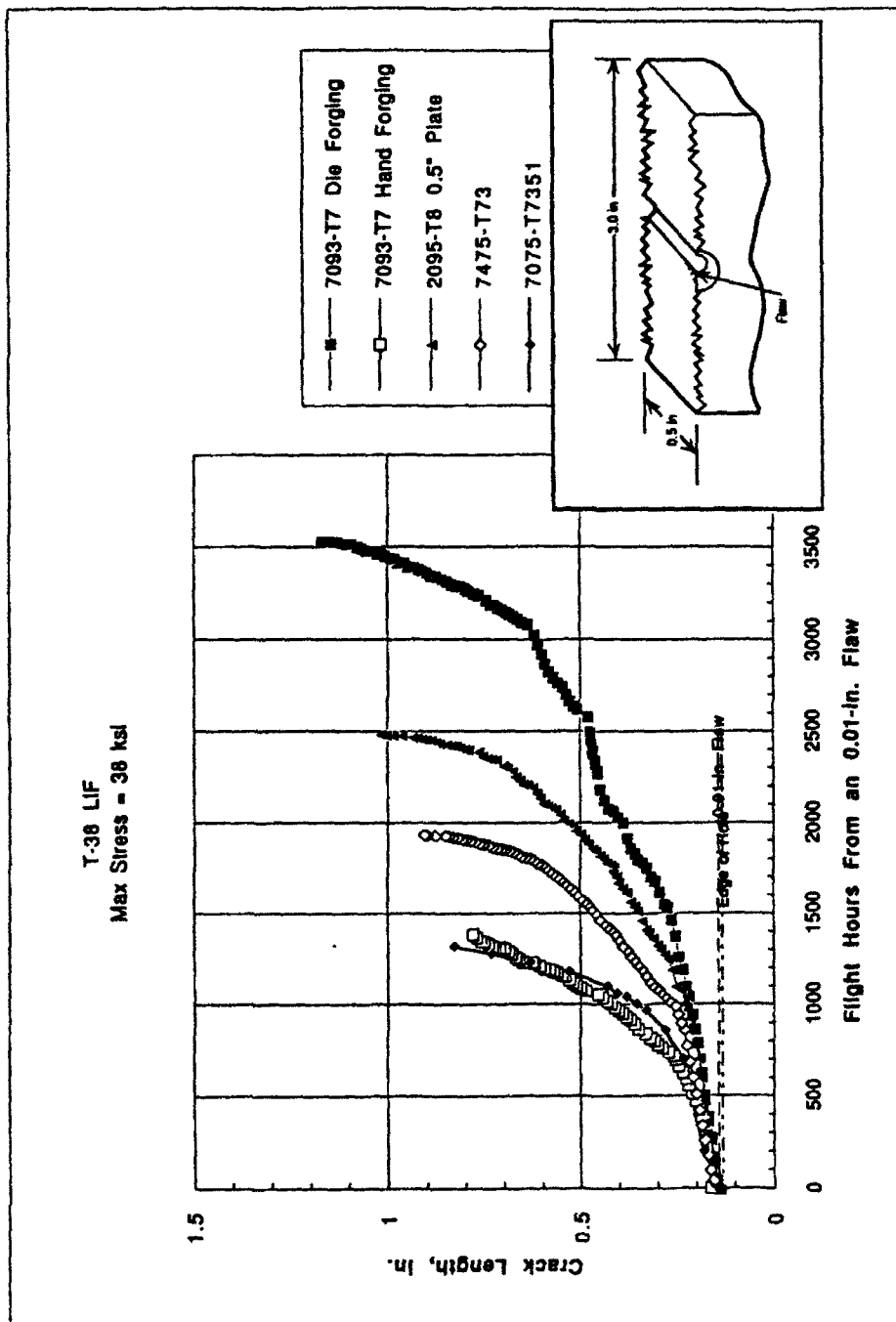
EvB/P	Crack (EvB/P)	Crack (visual)	Error	CAF
21.66	0.785	0.795	0.010	1.006
23.23	0.844	0.842	-0.002	1.005
28.22	1.003	0.990	-0.014	1.001
34.19	1.154	1.151	-0.003	0.998
36.97	1.213	1.219	0.005	0.997
46.28	1.377	1.379	0.002	0.993

## Comments

Date of test: 02-12-1992

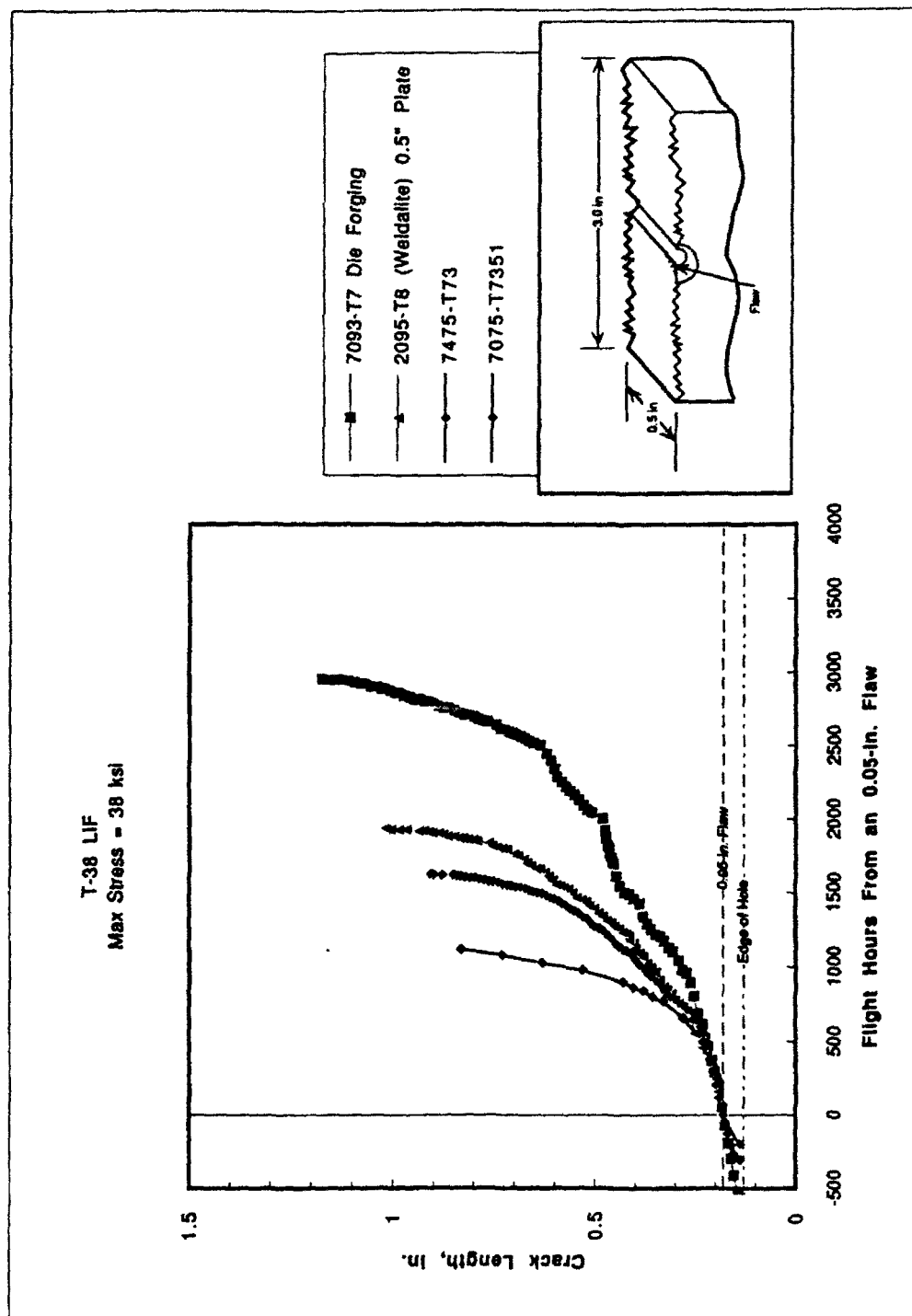
TABLE I36 (Continued)

Specimen Id. F2GT2				Page 1				Specimen Id. F2GT2				Page 2			
PNR	£48/P	a	N	AN	AS/AN	AK	AN	PNR	£48/P	a	N	AN	AS/AN	AK	AN
(lbs)		(in)	(X1)	(X1)	(in/cyc)	(ksi/in)	(X1)	(lbs)		(in)	(X1)	(X1)	(in/cyc)	(ksi/in)	(X1)
878	21.74	0.7885	326137	122269	1.957E-07	4.76	1816	1816	38.21	1.2378	1007739	1006	1.842E-05	14.38	1006
895	22.13	0.8035	405878	85112	2.094E-07	4.91	1842	1842	38.67	1.2467	1008195	842	1.995E-05	14.70	842
908	22.36	0.8124	448406	81995	2.162E-07	5.02	1869	1869	39.08	1.2546	1008581	808	2.135E-05	15.04	808
	22.60	0.8213	490989				1895	1895	39.58	1.2640	1009003	778	2.337E-05	15.36	778
	22.84	0.8301	530401				1922	1922	40.05	1.2728	1009359	693	2.428E-05	15.71	693
	23.15	0.8415	557757				1948	1948	40.50	1.2808	1009696	660	2.467E-05	16.05	660
951	23.34	0.8484	583768	59790	2.583E-07	5.39	1976	1976	40.95	1.2891	1010019	645	2.718E-05	16.40	645
964	23.59	0.8570	617547	66576	2.674E-07	5.62	2004	2004	41.48	1.2984	1010341	633	2.991E-05	16.77	633
978	23.84	0.8658	651275	64210	2.749E-07	5.74	2034	2034	42.03	1.3080	1010651	583	3.210E-05	17.17	583
992	24.10	0.8748	684123	62704	2.768E-07	5.87	2065	2065	42.56	1.3171	1010924	533	3.452E-05	17.58	533
1007	24.35	0.8835	715486	62694	2.804E-07	6.01	2095	2095	43.11	1.3264	1011184	495	3.648E-05	17.98	495
1022	24.61	0.8921	746827	51327	2.899E-07	6.14	2124	2124	43.64	1.3351	1011419	444	3.856E-05	18.39	444
1052	25.15	0.9099	808154	55847	3.018E-07	6.27	2154	2154	44.15	1.3435	1011628	419	4.059E-05	18.79	419
1068	25.39	0.9179	834027	50008	3.423E-07	6.42	2185	2185	44.69	1.3521	1011838	431	4.236E-05	19.23	431
1083	25.68	0.9270	858162	49275	3.744E-07	6.56	2215	2215	45.30	1.3618	1012059	435	4.284E-05	19.66	435
1100	25.97	0.9364	883302	45915	3.990E-07	6.71	2254	2254	45.88	1.3707	1012273	430	5.035E-05	20.22	430
1116	26.26	0.9453	904077	37374	4.673E-07	6.87	2281	2281	46.70	1.3898	1012489	318	5.992E-05	20.61	318
1133	26.54	0.9538	920676	31500	5.435E-07	7.02	2317	2317	47.12	1.3998	1012591	238	5.919E-05	21.14	238
1150	26.82	0.9625	935577	27552	6.575E-07	7.18	2345	2345	47.63	1.3975	1012727	270	6.259E-05	21.56	270
1168	27.14	0.9719	948228	21664	8.924E-07	7.35	2375	2375	48.26	1.4067	1012861	268	6.558E-05	22.00	268
1186	27.47	0.9818	957241	14654	1.254E-06	7.52	2408	2408	48.84	1.4153	1012995	254	7.262E-05	23.01	254
1204	27.77	0.9903	962882	10089	1.698E-06	7.70	2441	2441	49.47	1.4242	1013128	230	8.337E-05	24.11	230
1223	28.07	0.9989	967330	8338	2.182E-06	7.88	2476	2476	50.15	1.4337	1013249	204	9.139E-05	24.70	204
1240	28.40	1.0085	971220	6790	2.579E-06	8.04	2510	2510	50.84	1.4434	1013358	171	1.109E-04	25.27	171
1259	28.69	1.0164	974120	5587	2.926E-06	8.23	2547	2547	51.51	1.4524	1013454	155	1.228E-04	25.92	155
1276	28.99	1.0248	976807	5179	3.280E-06	8.40	2582	2582	52.25	1.4623	1013528	160	1.242E-04	26.56	160
1295	29.30	1.0334	979300	4905	3.567E-06	8.59	2622	2622	52.96	1.4715	1013609	147	1.426E-04	27.29	147
1314	29.64	1.0423	981712	4606	3.882E-06	8.78	2660	2660	53.79	1.4821	1013688	126	1.691E-04	27.94	126
1334	29.97	1.0513	983906	4206	4.226E-06	8.98	2703	2703	54.62	1.4925	1013756	102	1.921E-04	28.77	102
1354	30.31	1.0601	985918	3983	4.509E-06	9.19	2741	2741	55.51	1.5035	1013815	91	2.340E-04	29.68	91
1374	30.66	1.0693	987889	3677	4.803E-06	9.39	2789	2789	56.23	1.5121	1013859	100	4.411E-04	31.23	100
1394	31.00	1.0778	989594	3286	5.103E-06	9.60	2840	2840	57.29	1.5247	1013905	107	6.679E-04	33.69	107
1415	31.33	1.0860	991174	3197	5.429E-06	9.82	2925	2925	58.71	1.5409	1013954				
1435	31.69	1.0951	992791	3168	5.811E-06	10.04	3056	3056	61.26	1.5688	1014005				
1457	32.07	1.1044	994342	2901	6.237E-06	10.27			65.57	1.6124	1014061				
1479	32.44	1.1132	995692	2542	6.785E-06	10.50									
1500	32.79	1.1217	996884	2360	7.285E-06	10.74									
1523	33.17	1.1304	998052	2279	7.893E-06	10.98									
1545	33.57	1.1397	999163	2132	8.632E-06	11.23									
1593	33.97	1.1488	1000183	2047	9.359E-06	11.76									
1617	35.18	1.1756	1003210	3811	9.359E-06	12.03									
1663	35.59	1.1845	1003995	1463	1.136E-05	12.56									
1688	35.96	1.1922	1004673	1365	1.231E-05	12.85									
1711	36.39	1.2013	1005360	1369	1.312E-05	13.12									
1738	36.83	1.2102	1006043	1363	1.415E-05	13.45									
1762	37.34	1.2206	1006722	1147	1.571E-05	13.73									
1791	37.72	1.2282	1007189	1017	1.696E-05	14.08									



T-38 LIF & v. N 0.01" 4/24/92

Figure I13. T38 LIF Spectrum Fatigue Crack Growth Rate Data for 2095-T8 0.5 Inch Plate (Max Stress = 38 Ksi, Flaw = 0.01 inch). Northrop.



T-38 LIF a v. N 0.05" 5/8/92

Figure I14. T38 LIF Spectrum Fatigue Crack Growth Rate Data for 2095-T8 0.5 Inch Plate (Max Stress = 38 Ksi, Flaw = 0.05 inch). Northrop.

# T-38 LIF Spectrum Fatigue

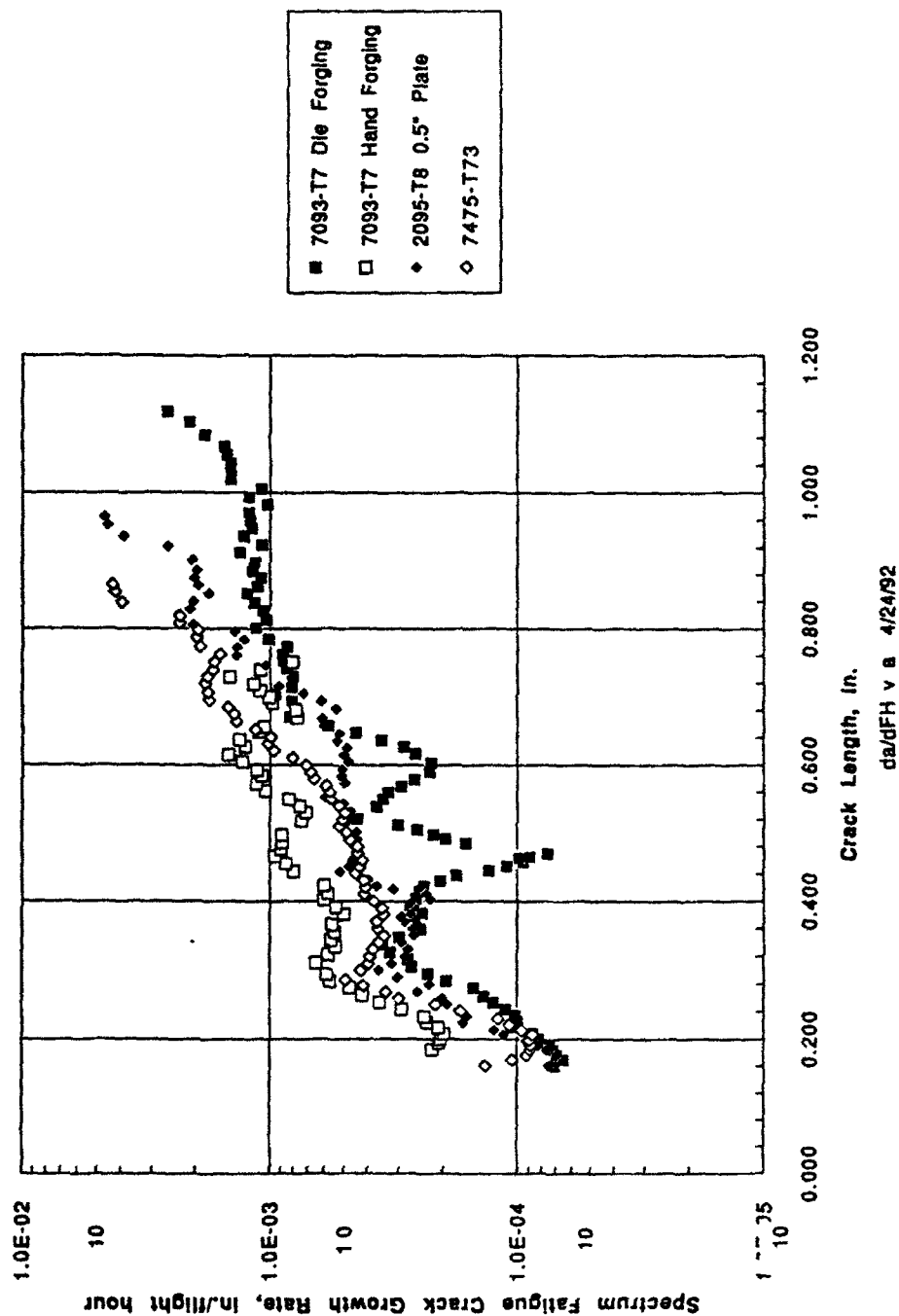


Figure I15. T38 LIF Spectrum Fatigue Crack Growth Rate Data for 2095-T8 0.5 Inch Plate (Max Stress = 38 Ksi). Northrop.

## SECTION V

### CONCLUSIONS

Seven aerospace laboratories participated in generating data on the 2095-T8 0.5-inch-thick plate for the cooperative test program. These data combined with previous interim reports on the Air Force/Industry Cooperative Test Program on Advanced Aluminum Alloys provide an extensive data base on aluminum-lithium alloys.